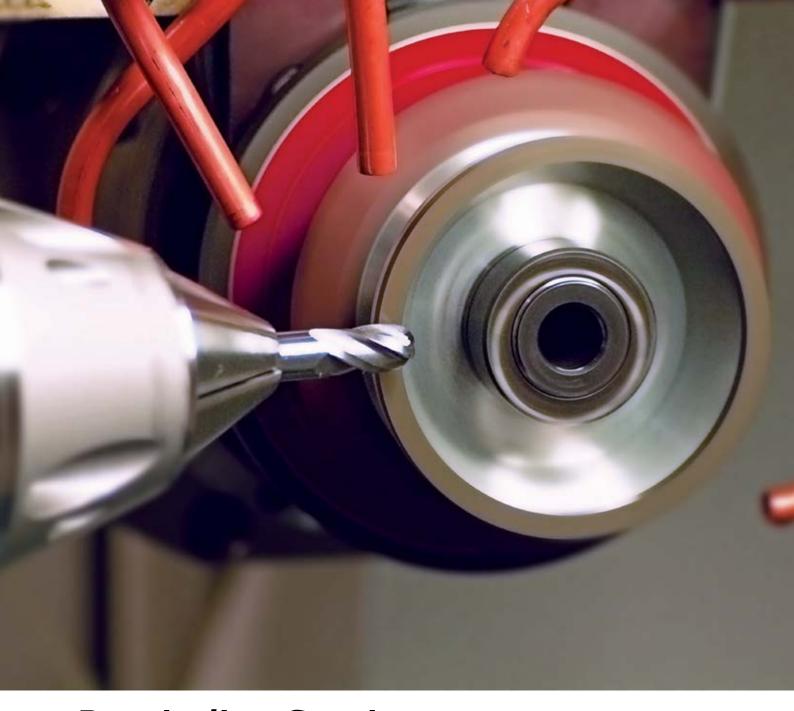


TECHNICAL INFO

- Speeds & Feeds Charts
 Troubleshooting
- General Drills Taps Endmills Reamers



Regrinding Service... Reduce your production costs

Sutton Tools continue to reinvest to provide a 'complete' range in cutting tool products and services. Our regrinding service returns tools to 'as new' condition. Quality is guaranteed from the CNC grinding machines which are operated by highly experienced personnel, using advanced technology. A full regrinding service is offered in Europe. HSS and carbide tooling can be reconditioned by our highly experienced personnel, with reproducible, high quality results, every time.

We regrind HSS Powdered Metallurgy and grades of Solid Carbide, complemented by fifth generation thin film coatings.

Sutton Tools Recoating Service

In Europe we provide a full regrinding service for Sutton Tools distributors. Using world-leading technology, coatings are available to solve a wide range of problems relating to friction and wear, thereby improving tool performance and increasing tool life, up to 300-1000% compared to uncoated.

Send & Return Service

Sutton Tools re-sharpening boxes will be provided for safe shipment of your tools for servicing. Simply fill in the request form, and we will return the tools to 'as new' condition as instructed. Contact us for your Sutton Tools re-sharpening box and request form.

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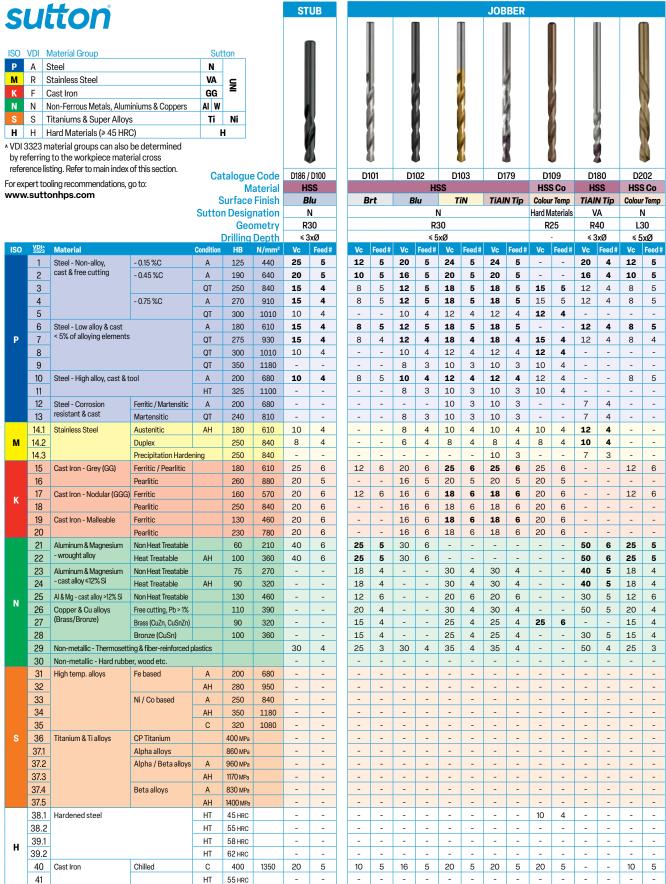
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| Mate | rial Group VDI^ | WKR | DIN | BS U.K. | EN U.K. | AFNOR | UNI | UNE | SS | JIS | AISI / SAE / UNS |
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| | 1 | 1.0737 | 9 SMnPb 36 | | | S300Pb | CF 9 SMnPb 36 | 12SMnP35 | 1926 | | 12 L 14, G 12144 |
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| | 10/11 | 1.2436 | X210 CrW 12 | | | | X 215 CrW 12 1 KU | F.5213 | 2312 | SKD 2 | D4 |
| | 10/11 | 1.2601 | X165 CrMoV 12 | | | 7.051115-011 | X 165 CrMoW 12 KU | | 2310 | | |
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| Mate | rial Group | WKR | DIN | BS | EN | AFNOR | UNI | UNE | SS | JIS | AISI / SAE / UNS |
|------|------------------|------------------|-------------------------------------|---------------------------------|------------|-------------------------------|------------------------------------|------------------|-----------|-----------------------|------------------------------------|
| ISO | VDI^ 3323 | Germany | Germany | U.K. | U.K. | France | Italy | Spain | Sweden | Japan | USA |
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| | 10/11 | 1.3348 | S 2-9-2 | | | Z 100 DCWV | HS 2-9-2 | HS 2-9-2 | 2782 | | M 7, T 11307 |
| | | | | DT 4 | | 09.04.02.02 Z 80 WKCV | | | - | CKITO | , , |
| | 10/11 | 1.3255 | \$18-1-2-5 | BT 4 | | 18.05.04.0 | HS 18-1-1-5 | HS 18-1-1-5 | | SKH3 | T 4, T 12004 |
| | 10/11 | 1.3355 | S 18-0-1 X45 CrSi 9-3 | BT 1 401 S 45 | 52 | Z 80 WCV 18.04.01 | HS 18-0-1 | HS 18-0-1 | | SKH 2 SUH 1 | T 1, T 12001 |
| | 10 /11 12 /13 | 1.4718 1.4104 | X45 CrMoS 17 | 401 S 45 420 S 37 | 32 | Z 45 CS 9 Z 10 CF 17 | X 45 CrSi 8 X 10 CrS 17 | F.3117 | 2383 | SUS 430 F | HNV 3, S 65007 430 F, S 43020 |
| Р | 12/13 | 1.4000 | X6 Cr 13 | 403 S 17 | | Z 6 C 13 | X 6 Cr 13 | F.3110 | 2301 | SUS 403 | 403. S 40300 |
| · | 12/13 | 1.4016 | X6 Cr 17 | 430 S 15 | 60 | Z8C17 | X 8 Cr 17 | F.3113 | 2320 | SUS 430 | 430, S 43000 |
| | 12/13 | 1.4113 | X6 CrMo 17 | 434 S 17 | | Z 8 CD 17.01 | X 8 CrMo 17 | | | SUS 434 | 434, S 43400 |
| | 12/13 | 1.4006 | X12 Cr 13 | 410 S 21 | 56A | Z10 C 13 | X 12 Cr 13 | F.3401 | 2302 | SUS 410 | 410 S, S 41000 |
| | 12/13 | 1.4001 | X7 Cr 14 | | | | | F.8401 | | SUS 429 | 429 |
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| | 12/13 | 1.4034 | X46 Cr 13 | 420 S 45 | 56D | Z 40 C 14 | X 40 Cr 14 | F.3405 | 2304 | SUS 420J2 | |
| | 12/13 | 1.4057 | X19 CrNi 17-2 | 431 S 29 | 57 | Z 15 CN 16.02 | X 16 CrNi 16 | F.3427 | 2321 | SUS 431 | 431, S 43100 |
| | 12/13 | 1.4313 | X3 CrNi 13-4 | 425 C 11 | | Z 5 CN 13.4 | X 6 CrNi 13 04 | | 2385 | SCS 5 | CA 6-NM, J 91540 |
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| | 14.1 | 1.4310 | X10 CrNi 18-8 | 301 S 21 | | Z 12 CN 17.07 | X2CrNi18 07 | F.3517 | 2331 | SUS 301 | 301, S 30100 |
| | 14.1 | 1.4401 | X5 CrNiMo 17-12-2 | 316 S 31 | 58J | Z 6 CND 17.11 | X 5 CrNiMo 17 12 | F.3543 | 2347 | SUS 316 | 316, S 31600 |
| | 14.1 | 1.4429 | X2CrNiMoN 17-13-3 | 316 S 62 | | Z 2 CND 17.13 Az | X 2 CrNiMoN 17 13 3 | | 2375 | SUS 316 LN | 316 LN, S 31653 |
| | 14.1 | 1.4583 | X6 CrNiMoNb 18-12 | | | | X 6 CrNiMoNb 17 13 | | | | 318 |
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| | 14.1 14.1 | 1.4301 1.4571 | X5 CrNi 18-10 X6 CrNiMoTi17-12-2 | 304 S 15 320 S 31 | 58E 58J | Z 6 CN 18.09 Z 6 CNT 17.12 | X 5 CrNi 18 11 | F.3504 F.3535 | 2332,2333 | SUS 304 SUS 316 Ti | 304 , 304 H, S 30400 |
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| | 14.2 | 1.4878 | X12 CrNiTi 18-9 | 321 \$ 51 | 58B | Z6CNT18.12B | | F.3523 | 2337 | 310 S SUS 321 | 321 |
| | 14.2 | 1.4541 | X14 CrNiTi 18-10 | 321 S 12 | 005 | Z 6 CNT 18.10 | X 6 CrNiTi 18 11 | F.3523 | 2337 | SUS 321 | 321 H, S 32100 |
| | 14.2 | 1.4550 | X6 CrNiNb 18-10 | 347 S 17 | 58F | Z 6 CNNb 18.10 | X 6 CrNiNb 18 11 | F.3524 | 2338 | SUS 347 | 347, S 34700 |
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| | 14.3 | 1.4542 | X5CrNiCuNb16-4 | | | Z6CNU17-04 | | | | | S17400, 17-4 PH; 630 |
| | 15/16 | 0.6020 | GG 20 | 180, 200/220, 220, Grade180, | | FGL200, Ft20D | G 20 | FG20 | 120 | FC200 | 200/225 250 20 200 |
| | 15/16 | 0.0020 | dd 20 | Grade260 | | FULZUU, FIZUD | G 20 | FGZU | 120 | FG200 | 200/225, 25B, 30, 30B |
| | 15 | 0.6010 | GG-10 | | 100 | FT 10 D | G10 | | 0110-00 | FC100 | |
| | 15 | 0.6015 | GG 15 | Grade 150 | | FT 15 D | G 15 | FG 15 | 0115-00 | FC150 | NO 25 B |
| | 15 | 0.6660 | GGL-NiCr202 | L-NiCuCr202 | | L-NC 202 | | | 0523-00 | | A436 Type 2 |
| | 15 | 0.7040 | GGG 40 | SNG 420/12 | | FCS 400-12 | GS400-12 | FGE 38-17 | 0717-02 | FCD400 | 60-40-18 300/325, 40B, |
| | 16 | 0.6030 | GG30 | Grade 300 | | Ft 30 D | G30 | FG30 | 01 30-00 | FC300 | 45/50, 45B |
| | 16 | 0.6035 | GG-35 | GRADE 350 | | Ft35D | G 35 | FG 35 | 135 | FC350 | A48-50 |
| | 16 | 0.6040 | GG40 | GRADE400 | | Ft 40 D | | | 140 | F0D700 | A48-60 B |
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| | 18 | 0.6025 | GG25 | Grade260 | | Ft 25 D | G25 | FG25 | 0717-12 | | S-NiCr20-2 250/275, 35, 35B, 40 |
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| | | 0.7000 | dddov | UNGUUU/3 | F14-001000 | 1 00000-3 | G25 | 1020 | | | 80-60-03 |
| | 18 | 0.8055 | GTW55 | | | | | | 0727-03 | FCD600 | A48 40 B |
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| | 19 | 0.8145 | GTS-45-06 | P 440/7 | | Mn 450-6 | | G10 00 | 0815-00 | | A220-40010 |
| | 19 | 5.0210 | GTS-35 | B 340/12 | | | 0852-00 | GMN 45 | 1310 00 | | |
| | 19 | | 55.55 | 8 290/6 | | MN 32-8 | | | | | |
| | 19 | | GTS-35 | B340/12 | | MN 35-10 | | | 0810-00 | | 32510 |
| | | | | | | | | | | | |

| | rial Group | WKR | DIN | BS | EN | AFNOR | UNI | UNE | SS | JIS | AISI / SAE / UNS |
|-----|----------------|------------------|-----------------------------|---------------------------|------|-------------------|------------------------|----------------|--------------|-----------------------|--------------------|
| ISO | VDI^ 3323 | Germany | Germany | U.K. | U.K. | France | Italy | Spain | Sweden | Japan | USA |
| | 20 | 0.8035 | GTM-35 | W340/3 | | MB35-7 MB40-10 | | | 814 | AC4A | |
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| | 20 | 0.8045 | GTMW-65 | | | | GMB40 | GTM 40 | 032 | | |
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| , X | 20 | 0.8165 | GTS-65-02 | P 570/3 | | Mn 650-3 | CIVID 10 | GIM 10 | 0854-00 | | 70003 |
| | 20 | 0.8170 | GTS-70-02 | P 690/2 | | Mn 700-2 | GMN 55, 65 | | 0854-00 | FCMP490 | 90001 |
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| | 22 | 3.1305 | AlCuMg0.5 | L86 | | A-U2G2117 | P-AlCu2.5MgSi | | | 2117 | 2117 |
| | 22 | 3.0517 | AlMnCu | | | | | | | | |
| | 23 | 3.2381 | G-AISi 10 Mg | G-AlSi9Mg | | A-S10G | | | AlSi10Mg | AC4A, ADC3 | A03590 |
| | 23 | 3.2382 | GD-AISi10Mg | | | | | | 811-04 | ADC3 | |
| | 23 | 3.2581 | G-AISi12 | LM20 | | A-S12U | G-AlSi13CuMn | | AlSi12Cu | AC3A | A04130 |
| | 23 | 3.3561 | G-AIMg 5 | | | | | | | AC7A, ADC5, Al-Mg6 | |
| | 23 | 3.5101 | G-MgZn4sE1Zr1 | MAG 5 | | | | | | | ZE 41 |
| | 23 | 3.5103 | MgSE3Zn27r1 | MAG 6 | | G-TR3Z2 | | | | | EZ 33 |
| | 23 | 3.5812 | G-MgAl8Zn1 | NMAG 1 | | | | | | | AZ 81 |
| | 23 | 3.5912 | G-MgAl9Zn1 | MAG 7 | | | | | | | AZ 91 |
| | 23 | 3.3549 | AlMg5Mn | | | | | | | | |
| | 23 | 3.3555 | AlMg5 | | | | | | | | |
| | 23 | 3.3547 | AlMg4.5, AlMg4.5Mn | 5083 | | 5183 | P-AlMg4.4 | | AlMg4.5Mn | 5082 | A95083 |
| | 23-24 23-24 | 3.2383 | G-AlSi0Mg(Cu) | LM9 2789;1973 | | NF A32-201 | | | 4253 | | A360.2 A356-72 |
| | 23-24 | | | LM25 | | INI AGE-201 | | | 4244 | A5052 | 356.1 |
| N | 23-24 | | G-AlSi12 | LM 6 | | | | | 4261 | HOULE | A413.2 |
| IN | 23-24 | | G-AlSi 12 (Cu) | LM 20 | | | | | 4260 | ADC12 | A413.1 |
| | 23-24 | | GD-AISi12 | | | | | | 4247 | A6061 | A413.0 |
| | 23-24 | | GD-AlSi8Cu3 | LM24 | | | | | 4250 | A7075 | A380.1 |
| | 24 | 2.1871 | G-AICu 4 TiMg | | | | | | | | |
| | 24 | 3.1754 | G-AlCu5Ni1,5 | | | | | | | | |
| | 24 | 3.2163 | G-AlSi9Cu3 | | | | | | | ADC10 | |
| | 24 | 3.2371 | G-AISi 7 Mg | | | | | | | AC4CH | 4218 B |
| | 24 | 3.2373 | G-AISI9MGWA | | | A-S7G | | | 4251 | C4BS | SC64D |
| | 24 | 3.5106 | G-MgAg3SE2Zr1 | mag 12 | | | | | | | QE 22 |
| | 24 | 0.4000 | G-ALMG5 | LM5 | | A-SU12 | | | 4252 | | GD-AISI12 |
| | 26 | 2.1090 | G-CuSn 7 5 pb | 100 | | U-E 7 Z 5 pb 4 | | | | | C93200 |
| | 26 | 2.1096 2.1098 | G-CuSn5ZnPb | LG 2 | | | | | | | c 83600 C 83600 |
| | 26 26 | 2.1098 | G-CuSn 2 Znpb G-CuPb15Sn | LB1 | | U-pb 15 E 8 | | | | | C23000 |
| | 27 | 2.0240 | G-CuPbioSii CuZn 15 | LUI | | O PU IO E O | | | | | 020000 |
| | 27 | 2.0321 | CuZn 37 | cz 108 | | CuZn 36, CuZn 37 | C 2700 | | | | C27200 |
| | 27 | 2.0590 | G-CuZn40Fe | , | | 22, 302.101 | | | | | |
| | 27 | 2.0592 | G-CuZn 35 Al 1 | U-Z 36 N 3 | | HTB1 | | | | | C 86500 |
| | 27 | 2.1293 | CuCrZr | CC 102 | | U-Cr 0.8 Zr | | | | | C 18200 |
| | 28 | 2.0060 | E-Cu57 | | | | | | | | |
| | 28 | 2.0375 | CuZn36Pb3 | | | | | | | | |
| | 28 | 2.0966 | CuAl 10 Ni 5 Fe 4 | Ca 104 | | U-A 10 N | | | | | C 63000 |
| | 28 | 2.0975 | G-CuAl 10 Ni | | | | | | | | B-148-52 |
| | 28 | 2.1050 | G-CuSn 10 | CT1 | | | | | | | c 90700 |
| | 28 | 2.1052 | G-CuSn 12 | pb 2 | | UE 12 P | | | | | C 90800 |
| | 28 | 2.1292 | G-CuCrF 35 | CC1-FF | | | | | | | C 81500 |
| | 28 | 2.4764 | CoCr20W15Ni | | | | | | | | |

| Mate | rial Group | WKR | DIN | BS | EN | AFNOR | UNI | UNE | SS | JIS | AISI / SAE / UNS |
|------|--------------|---------|-----------------------|--------------------|------|----------------|---------------|--------------|--------|---------|----------------------|
| ISO | VDI^ 3323 | Germany | Germany | U.K. | U.K. | France | Italy | Spain | Sweden | Japan | USA |
| 130 | 3323 | 1.4558 | X 2 NiCrAITi 32 20 | 0.K. NA 15 | U.K. | France | Italy | Spain | Sweden | Japan | N 08800 |
| | 31 | 1.4562 | X1NiCrMoCu 32 28 7 | IVAID | | | | | | | N 08031 |
| | | 1.4563 | X 1 NiCrMoCuN 3127 4 | | | | | | 2584 | | N 08028 |
| | 31 | | | NA 17 | | 7 10 NOC 05 10 | | | 2084 | CULLOOO | |
| | 31 | 1.4864 | X 12 NiCrSi 36 16 | NA 17 | | Z 12 NCS 35.16 | VOE0NIO-00 10 | | | SUH 330 | INCOLOY DS,, N08330 |
| | 31 | 1.4865 | G-X40NiCrSi38 18 | 330 C 40 | | | XG50NiCr39 19 | | | SCH15 | N 08004 |
| | 31 | 1.4958 | X 5 NiCrAITi 31 20 | | | | | | | | |
| | 31 | 2.4668 | NiCr19NbMo | | | NC20K14 | | | | | AMS 5544 |
| | 32 | 1.4977 | X 40 CoCrNi 20 20 | | | Z 42 CNKDWNb | | | | | |
| | 33 | 2.4360 | NiCu30Fe | NA 13 | | NU 30 | | | | | Monel 400 |
| | 33 | 2.4603 | | | | NC22FeD | | | | | 5390A |
| | 33 | 2.4610 | NiMo16cR16Ti | | | | | | | | Hastelloy C-4 |
| | 33 | 2.4630 | NiCr20Ti | HR 5,203-4 | | NC 20 T | | | | | Nimonic 75 |
| | 33 | 2.4642 | NiC29Fe | | | Nnc 30 Fe | | | | | Inconel 690 |
| | 33 | 2.4856 | NiCr22Mo9Nb | NA 21 | | NC 22 FeDNb | | | | | INCONEL 625, N 26625 |
| | 33 | 2.4858 | NiCr21Mo | NA 16 | | NC 21 Fe DU | | | | | Incoloy 825 |
| | 34 | 2.4375 | NiCu30 Al | NA 18 | | NU 30 AT | | | | | Monel k-500 |
| | 34 | 2.4631 | NiCr20TiAI | Hr40;601, NA 20 | | NC20TA | | | | | N 07080 |
| | 34 | 2.4668 | NiCr19FeNbMo | TUTEO | | NC 19 Fe Nb | | | | | Inconel 718 |
| | 34 | 2.4694 | NiCr16fE7TiAl | | | | | | | | Inconel |
| | 34 | 2.4955 | NiFe25Cr20NbTi | | | | | | | | |
| | 34 | 2.4668 | NiCr19Fe19NbMo | HR8 | | NC19eNB | | | | | 5383 |
| s | 34 | 2 4670 | S-NiCr13A16MoNb | 3146-3 | | NC12AD | | | | | 5391 |
| | 34 | 2.4662 | NiFe35Cr14MoTi | 0110 0 | | ZSNCDT42 | | | | | 5660 |
| | 34 | 2.4964 | CoCr20W15Ni | | | KC20WN | | | | | 5537C |
| | 34 | 2.4304 | C0Cr22W14Ni | | | KC22WN | | | | | AMS 5772 |
| | 34 | | COCIZZWIANI | | | ROZZWIN | | | | | N07725, Inconel 725 |
| | | 2.4669 | NiCr15Fe7TiAl | | | NC 15 TNb A | | | | | Inconel X-750 |
| | 35 | | | | | NC IS TND A | | | | | |
| | 35 | 2.4685 | G-NiMo28 | | | | | | | | Hastelloy B |
| | 35 | 2.4810 | G-NiMo30 | | | NOTOKOT | | | | | Hastelloy C |
| | 35 | 2.4973 | NiCr19Co11MoTi | | | NC19KDT | | | | | AMS 5399 |
| | 35 | 3.7115 | TiAl5Sn2 | | | | | | | | |
| | 36 | 3.7025 | Ti1 | 2 TA 1 | | | | | | | R 50250 |
| | 36 | 3.7225 | Ti1pd | TP1 | | | | | | | R 52250 |
| | 36 | 2 4674 | NiCo15Cr10MoAlTi | | | | | | | | AMS 5397 |
| | 37 | 3.7124 | TiCu2 | 2 TA 21-24 | | | | | | | |
| | 37 | 3.7145 | TiAl6Sn2Zr4Mo2Si | | | | | | | | R 54620 |
| | 37 | 3.7165 | TiAl6V4 | TA 10-13;TA 28 | | T-A 6 V | | | | | |
| | 37 | 3.7185 | TiAl4Mo4Sn2 | TA 45-51; TA 57 | | | | | | | |
| | 37 | 3.7195 | TiAl 3 V 2.5 | | | | | | | | |
| | 37 | | TiAl4Mo4Sn4Si0.5 | | | | | | | | |
| | 37 | | TiAl5Sn2.5 | TA14/17 | | T-A5E | | | | | AMS R54520 |
| | 37 | | TiAl6V4 | TA10-13/TA28 | | T-A6V | | | | | AMS R56400 |
| | 37 | | TiAl6V4ELI | TA11 | | | | | | | AMS R56401 |
| | 38 | 1.1545 | C 105 W1 | BW 1A | | Y1 105 | C 100 KU | F-5118 | 1880 | SK 3 | W1 |
| | 38 | 1.2762 | 75 CrMoNiW 6 7 | | | | | | | | |
| | 38 | 1.4125 | X105 CrMo 17 | | | Z 100 CD 17 | | | | | 440C |
| | 38 | 1.6746 | 32 nlcRmO 14 5 | 832 M 31 | | 35 NCD 14 | | | | | <u> </u> |
| | 40 | 0.9620 | G-X 260 NiCr 4 2 | Grade 2 A | | | 0512-00 | | | | Ni- Hard 2 |
| | 40 | 0.9625 | G-X 330 Ni Cr 4 2 | Grade 2 B | | | | | | | Ni- Hard 1 |
| н | 40 | 0.9630 | G-X 300 CrNiSi 9 5 2 | | | | 0513-00 | | | | Ni-Hard 4 |
| " | 40 | 0.9640 | G-X 300 CrMoNi 15 2 1 | | | | | | | | |
| | 40 | 0.9650 | G-X 260 Cr 27 | Grade 3 D | | | | | | | A 532 III A 25% Cr |
| | 40 | 0.9655 | G-X 300 CrNMo 27 1 | Grade 3 E | | | | | | | A 532 III A 25% Cr |
| | 40 | 1.2419 | 105 WCr 6 | 105WC13 | | | 0466-00 | | | | |
| | 40 | 1.4841 | X15 CrNiSi 25 20 | 314 S31 | | Z 15 CNS 25-20 | | | | | 310 |
| | 41 | 0.9635 | G-X 300 CrMo 15 3 | | | | | | | | |
| | 41 | 0.9645 | G-X 260 CrMoNi 20 2 1 | | | | | 107 WCr 5 KU | | | |



Condition: A (Annealed), AH (Age Hardened), C (Cast), HT (Hardened & Tempered), QT (Quenched & Tempered)
Bold = Optimal | Regular = Effective

Notes on Drilling

- 1. Step feeding or pecking is required for drilling greater than $3 \times \emptyset$.
- 2. When drilling cast surface & black (ie: not machined surface), reduce drilling speed by 20%.
- 3. For optimal positional accuracy and hole size, the use of spot drills is recommended prior to drilling desired hole, refer to our standard range (D175).
- 4. For hole depths greater than $7 \times \emptyset$, pre-drill initially to pilot start for more accurate hole position and eliminate drill wandering. The pilot can be drilled with short rigid drill, approximately. $3 \times \emptyset$ in depth and reduced feed to ensure accurate pilot hole.



| | Feed Table (f) (mm/rev) | | | | | | | | | | | | |
|------|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|------|--|--|--|
| ~ | Feed # | | | | | | | | | | | | |
| Ø | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | | |
| 2.0 | 0.020 | 0.025 | 0.030 | 0.040 | 0.050 | 0.060 | 0.075 | 0.095 | 0.120 | 0.15 | | | |
| 3.0 | 0.030 | 0.035 | 0.045 | 0.055 | 0.070 | 0.090 | 0.110 | 0.135 | 0.17 | 0.21 | | | |
| 4.0 | 0.040 | 0.045 | 0.060 | 0.075 | 0.090 | 0.115 | 0.140 | 0.18 | 0.22 | 0.27 | | | |
| 5.0 | 0.045 | 0.055 | 0.070 | 0.090 | 0.110 | 0.135 | 0.17 | 0.21 | 0.26 | 0.32 | | | |
| 6.0 | 0.055 | 0.065 | 0.080 | 0.100 | 0.125 | 0.16 | 0.19 | 0.24 | 0.30 | 0.37 | | | |
| 8.0 | 0.070 | 0.085 | 0.105 | 0.130 | 0.16 | 0.20 | 0.25 | 0.31 | 0.38 | 0.47 | | | |
| 10.0 | 0.085 | 0.105 | 0.125 | 0.16 | 0.19 | 0.24 | 0.30 | 0.37 | 0.46 | 0.56 | | | |
| 12.0 | 0.095 | 0.120 | 0.15 | 0.18 | 0.23 | 0.28 | 0.34 | 0.42 | 0.52 | 0.64 | | | |
| 16.0 | 0.125 | 0.15 | 0.19 | 0.23 | 0.29 | 0.36 | 0.44 | 0.54 | 0.66 | 0.82 | | | |
| 20.0 | 0.15 | 0.18 | 0.23 | 0.28 | 0.34 | 0.42 | 0.52 | 0.64 | 0.80 | 0.98 | | | |
| 25.0 | 0.18 | 0.22 | 0.27 | 0.33 | 0.41 | 0.50 | 0.60 | 0.74 | 0.90 | 1.10 | | | |
| 32.0 | 0.23 | 0.27 | 0.33 | 0.41 | 0.50 | 0.60 | 0.74 | 0.88 | 1.10 | 1.30 | | | |
| 38.0 | 0.26 | 0.32 | 0.38 | 0.46 | 0.56 | 0.68 | 0.82 | 1.00 | 1.20 | 1.45 | | | |
| 45.0 | 0.30 | 0.36 | 0.43 | 0.52 | 0.64 | 0.76 | 0.92 | 1.10 | 1.35 | 1.60 | | | |
| 52.0 | 0.33 | 0.40 | 0.48 | 0.58 | 0.70 | 0.84 | 1.00 | 1.20 | 1.45 | 1.75 | | | |
| 63.0 | 0.39 | 0.47 | 0.56 | 0.67 | 0.80 | 0.96 | 1.14 | 1.35 | 1.65 | 1.95 | | | |

| METRIC DRILLS (mm size) | | | | | | | |
|-------------------------|---|------------------|--------------------------------|---|--|--|--|
| Ø | = nominal tap size (mm) | n= | v _c × 1000 Ø × π | $- \simeq \frac{V_c}{\emptyset} \times 318$ | | | |
| n Vo f | = spindle speed (RPM) = cutting speed (m/min) = feed (mm/rev) | v _c = | n x Ø × π 1000 | - ≃ <u>n x Ø</u> 318 | | | |
| Vf | = feed rate (mm/min) | v _f = | fxn | | | | |

| ISO | VDI | Material Group | | Sut | ton |
|-----|-----|--|----|-----|-----|
| Р | Α | Steel | 1 | ١ | |
| М | R | Stainless Steel | ٧ | Ά | Ξ |
| K | F | Cast Iron | G | Z | |
| N | N | Non-Ferrous Metals, Aluminiums & Coppers | ΑI | W | |
| S | S | Titaniums & Super Alloys | 1 | ï | Ni |
| Н | Н | Hard Materials (≥ 45 HRC) | | ŀ | ł |

A VDI 3323 material groups can also be determined by referring to the workpiece material cross reference listing. Refer to main index of this section.

For expert tooling recommendations, go to: www.suttonhps.com

| FOR BLIND & TH | IROUGH HOLES |
|---------------------------|--------------|
| | |
| T384 / T385 / T386 / T901 | |
| T401 / T402 / T403 / T902 | T404 |

T476

Catalogue Code M MF T414/ T415/ T416/ T903 UNF T431 / T432 / T433 / T904 BSW T451 / T452 / T453 / T905 BSF, BA, BSB (Brass) T466 / T467 / T468 / T906 G(BSPF) T479/ T480/ T481/ T909 T482 / T483 **BSPT** T475

Material Surface Finish Brt TiN

| | | | | | Surrace | | Brt | IIN |
|-----|--------------|------------------------------------|------------------------|-----------|----------|--------|--------------|-----|
| | | | | Sutto | on Desig | nation | P | N |
| | | | | | Geo | metry | | |
| | | | | | Thread | Depth | ≤1 | xØ |
| ISO | VDIA 3323 | Material | | Condition | НВ | N/mm² | Vc (m | |
| | 1 | Steel - Non-alloy, | - 0.15 %C | Α | 125 | 440 | 7 | 11 |
| | 2 | cast & free cutting | - 0.45 %C | A | 190 | 640 | 7 | 11 |
| | | | ~ 0.40 %0 | | | | , | |
| | 3 | | | QT | 250 | 840 | 6 | 9 |
| | 4 | | ~ 0.75 %C | Α | 270 | 910 | 7 | 10 |
| | 5 | | | QT | 300 | 1010 | 5 | 8 |
| | 6 | Steel - Low alloy & cast | | Α | 180 | 610 | 7 | 11 |
| P | 7 | < 5% of alloying elements | | QT | 275 | 930 | 5 | 7 |
| | 8 | | | QT | 300 | 1010 | 4 | 5 |
| | 9 | | | QT | 350 | 1180 | _ | - |
| | 10 | Steel - High alloy, cast & to | nol | A | 200 | 680 | 5 | 7 |
| | 11 | otoor riigiralloy, cast a t | 501 | HT | 325 | 1100 | _ | - |
| | | Otrad Ormanian | Familia (Mantanaliia | | | | <u>-</u> | |
| | 12 | Steel - Corrosion resistant & cast | Ferritic / Martensitic | Α | 200 | 680 | | |
| | 13 | | Martensitic | QT | 240 | 810 | - | - |
| | 14.1 | Stainless Steel | Austenitic | AH | 180 | 610 | - | - |
| M | 14.2 | | Duplex | | 250 | 840 | = | - |
| | 14.3 | | Precipitation Harde | ning | 250 | 840 | - | - |
| | 15 | Cast Iron - Grey (GG) | Ferritic / Pearlitic | | 180 | 610 | 7 | 11 |
| | 16 | | Pearlitic | | 260 | 880 | 6 | 9 |
| | 17 | Cast Iron - Nodular (GGG) | | | 160 | 570 | 7 | 11 |
| K | 18 | odociion itoddia (dda) | Pearlitic | | 250 | 840 | 6 | 9 |
| | 19 | Cast Iron - Malleable | | | | | 9 | 14 |
| | | Cast from - Malleable | Ferritic | | 130 | 460 | | |
| | 20 | | Pearlitic | | 230 | 780 | 7 | 11 |
| | 21 | Aluminum & Magnesium | Non Heat Treatable | | 60 | 210 | 7 | 11 |
| | 22 | - wrought alloy | Heat Treatable | AH | 100 | 360 | 9 | 14 |
| | 23 | Aluminum & Magnesium | Non Heat Treatable | | 75 | 270 | 9 | 14 |
| | 24 | - cast alloy ≤12% Si | Heat Treatable | AH | 90 | 320 | 9 | 14 |
| | 25 | Al & Mg - cast alloy >12% Si | Non Heat Treatable | | 130 | 460 | - | - |
| N | 26 | Copper & Cu alloys | Free cutting, Pb > 1% | | 110 | 390 | 5 | 7 |
| | 27 | (Brass/Bronze) | Brass (CuZn, CuSnZn) | | 90 | 320 | 11 | 16 |
| | 28 | | Bronze (CuSn) | | 100 | 360 | 8 | 13 |
| | 29 | Non-motallic Thormes att | | plactics | 100 | 550 | - | - |
| | | Non-metallic - Thermosetti | | JIASLICS | | | <u>-</u> | - |
| | 30 | Non-metallic - Hard rubbe | | | 200 | 24. | | |
| | 31 | High temp. alloys | Fe based | A | 200 | 680 | - | - |
| | 32 | | | AH | 280 | 950 | - | - |
| | 33 | | Ni / Co based | Α | 250 | 840 | - | - |
| | 34 | | | AH | 350 | 1180 | - | - |
| | 35 | | | С | 320 | 1080 | - | - |
| S | 36 | Titanium & Ti alloys | CP Titanium | | 400 MPa | | - | - |
| | 37.1 | | Alpha alloys | | 860 MPa | | - | - |
| | 37.2 | | Alpha / Beta alloys | Α | 960 MPa | | _ | _ |
| | 37.3 | | Alpha / Deta alloys | AH | 1170 MPa | | _ | _ |
| | | | Data allay: | | | | - | - |
| | 37.4 | | Beta alloys | Α | 830 MPa | | | |
| | 37.5 | | | AH | 1400 MPa | | - | - |
| | 38.1 | Hardened steel | | HT | 45 HRC | | - | - |
| | 38.2 | | | HT | 55 HRC | | - | - |
| н | 39.1 | | | HT | 58 HRC | | - | - |
| п | 39.2 | | | HT | 62 HRC | | - | - |
| | 40 | Cast Iron | Chilled | С | 400 | 1350 | - | - |
| | //1 | | | LIT | FFUDO | | | |

| FOR T | HROUGH I | OLES |
|--------------|---------------------|-----------------|
| | | |
| T393 | T394 | T395 |
| T406 | T407 | T408 |
| T422 | T423 | T424 |
| T439 T457 | T440 T458 | T441 T459 |
| - | - | - |
| T484 | - | - |
| - | - UCCE | - |
| Brt | HSSE Blu | TiN |
| | N | |
| | | |
| | ≤ 3xØ Vc (m/min) | |
| 12 | 13 | 18 |
| 12 | 13 | 18 |
| 10 | 11 | 15 |
| 11 | 12 | 17 |
| - 12 | 13 | 14 18 |
| 8 | 9 | 12 |
| - | - | 9 |
| - | - | - |
| 8 | 9 | 12 |
| - | - | - |
| - | 6 | - 8 |
| - | 7 | 9 |
| - | 4 | 6 |
| - | 3 | 5 |
| 12 | 13 | 18 |
| 12 | - 13 | 15 18 |
| - | - | 15 |
| 15 | 17 | 23 |
| 12 | 13 | 18 |
| 12 | - | 18 |
| 15 | - | 23 23 |
| 15 | - | 23 |
| - | - | - |
| 8 | - | 12 |
| 18 | - | 27 - |
| - | - | - |
| - | - | - |
| - | - | - |
| - | - | - |
| - | - | - |
| - | - | - |
| - | - | - |
| - | - | - |
| - | - | - |
| - | - | - |
| - | - | - |
| - | - | - |
| = | - | - |
| - | - | - |
| - | - | - |

 $\textbf{Condition: A} \ (\textbf{Annealed}), \ \textbf{AH} \ (\textbf{Age Hardened}), \ \textbf{C} \ (\textbf{Cast}), \ \textbf{HT} \ (\textbf{Hardened} \ \& \ \textbf{Tempered}), \ \textbf{QT} \ (\textbf{Quenched} \ \& \ \textbf{Tempered})$ **Bold =** Optimal | Regular = Effective



Notes on Tapping

VDIA 3323

N

Н

- 1. The speeds listed above are a recommendation only, and are based on depth of thread listed, speeds can be adjusted on application. As a general rule;
 - -If hole depth required is less than above mentioned = increase speed -If hole depth required is more than above mentioned = reduce speed
- 2. Taps must be driven by the square to eliminate slippage, eg, ER-GB collets (square drive).
- 3. When using spiral flute taps with length compensation tapping attachment, it is recommended to short pitch the feed 95%, to eliminate tap cutting oversize, eg. M6x1 @ 1000RPM, Feedrate= 950mm/min.

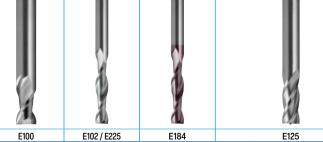
| | METRIC TAPS (mm size) | | | | | | | | | | | | | |
|----------------------------------|--|-------------------------|--------------------------------------|---|--|--|--|--|--|--|--|--|--|--|
| Ø P | = nominal tap size (mm) = thread pitch (mm) | n= | <u>v_c × 1000</u> Ø × π | $\simeq \frac{V_c}{\varnothing} \times 318$ | | | | | | | | | | |
| n Vc | = spindle speed (RPM) = cutting speed (m/min) = feed rate (mm/min) | v _c = | <u>nxØ×π</u> 1000 | $- \simeq \frac{n \times \emptyset}{318}$ | | | | | | | | | | |
| V _f V _r | = feed rate per rev (mm/rev) | v _f = | nxP | | | | | | | | | | | |

 $\textbf{Condition: A} \ (\textbf{Annealed}), \ \textbf{AH} \ (\textbf{Age Hardened}), \ \textbf{C} \ (\textbf{Cast}), \ \textbf{HT} \ (\textbf{Hardened} \ \& \ \textbf{Tempered}), \ \textbf{QT} \ (\textbf{Quenched} \ \& \ \textbf{Tempered})$ **Bold = Optimal | Regular = Effective**

| ISO | VDI | Material Group | Sutton | | | |
|-----|-----|--|--------|---|----|--|
| Р | Α | Steel | 1 | ١ | | |
| М | R | Stainless Steel | ٧ | Ά | S | |
| K | F | Cast Iron | G | G | 2 | |
| N | N | Non-Ferrous Metals, Aluminiums & Coppers | ΑI | W | | |
| S | S | Titaniums & Super Alloys | 1 | ī | Ni | |
| Н | Н | Hard Materials (≥ 45 HRC) | | ŀ | ŀ | |

NOI 3323 material groups can also be determined by referring to the workpiece material cross reference listing. Refer to main index of this section.

For expert tooling recommendations, go to: **www.suttonhps.com**



Catalogue Code HSS Co.8 Material HSS Co.8 HSS Co.8 Surface Finish Brt Brt TiAIN Brt **Sutton Designation** Ν Geometry R30 R30 R30 Type of Cut: Slotting Finishing Universal Roughing **Profiling** ‡ apר 0.5 0.5 0.5 1.5 1.5 → ae × Ø 1.0 1.0 0.1 1.0 0.25

| ISO | VDIA 3323 | Material | | Condition | НВ | N/mm² | Vc | Feed# |
|-----|--------------|---|--------------------------|-----------|----------|-------|----|-------|----|-------|----|-------|----|-------|----|-------|
| 100 | 1 | Steel - Non-alloy, | ~ 0.15 %C | A | 125 | 440 | 30 | 6 | 18 | 5 | 22 | 5 | 40 | 4 | 40 | 5 |
| | 2 | cast & free cutting | ~ 0.45 %C | | 190 | 640 | 30 | 6 | 18 | 5 | 22 | 5 | 40 | 4 | 40 | 5 |
| | 3 | oute a not carring | ~ 0.45 %C | A | | | 30 | 6 | 18 | 5 | 22 | 5 | 40 | 4 | 40 | 5 |
| | 4 | | ~ 0.75 %C | QT | 250 | 840 | 30 | 6 | 18 | 5 | 22 | 5 | 40 | 4 | 40 | 5 |
| | 5 | | ~ 0.75 %C | A | 270 | 910 | 20 | 5 | 12 | 4 | 15 | 4 | 25 | 3 | 25 | 4 |
| | | 0 | | QT | 300 | 1010 | | 6 | | | 22 | 5 | | 4 | 40 | 5 |
| Р | 6 | Steel - Low alloy & cast < 5% of alloying elements | | Α | 180 | 610 | 30 | | 18 | 5 | | 4 | 40 | 3 | | 4 |
| Р | 7 | - 576 Of alloying cicinicitis | | QT | 275 | 930 | 25 | 5 | 15 | 4 | 18 | 4 | 30 | | 30 | 4 |
| | 8 | | | QT | 300 | 1010 | 20 | 5 | 12 | | 15 | | 25 | 3 | 25 | |
| | 9 | | | QT | 350 | 1180 | - | - | - | - | - | - | - | - | - | - |
| | 10 | Steel - High alloy, cast & t | ool | A | 200 | 680 | 20 | 5 | 12 | 4 | 15 | 4 | 25 | 3 | 25 | 4 |
| | 11 | | | HT | 325 | 1100 | - | - | - | - | - | - | - | - | - | - |
| | 12 | Steel - Corrosion | Ferritic / Martensitic | Α | 200 | 680 | - | - | - | - | 11 | 4 | 10 | 2 | 10 | 3 |
| | 13 | resistant & cast | Martensitic | QT | 240 | 810 | 15 | 4 | 9 | 3 | 11 | 3 | 22 | 3 | 22 | 4 |
| | 14.1 | Stainless Steel | Austenitic | AH | 180 | 610 | - | - | - | - | 11 | 4 | - | - | - | - |
| M | 14.2 | | Duplex | | 250 | 840 | - | - | - | - | 9 | 2 | - | - | - | - |
| | 14.3 | | Precipitation Harde | ning | 250 | 840 | - | - | - | - | - | - | - | - | - | - |
| | 15 | Cast Iron - Grey (GG) | Ferritic / Pearlitic | | 180 | 610 | 30 | 5 | 18 | 4 | 21 | 4 | 35 | 3 | 35 | 4 |
| | 16 | | Pearlitic | | 260 | 880 | 25 | 4 | 15 | 3 | 18 | 3 | 25 | 2 | 25 | 3 |
| К | 17 | Cast Iron - Nodular (GGG) | Ferritic | | 160 | 570 | 20 | 3 | 12 | 2 | 15 | 2 | 22 | 2 | 22 | 3 |
| 1. | 18 | | Pearlitic | | 250 | 840 | 20 | 3 | 12 | 2 | 15 | 2 | 22 | 2 | 22 | 3 |
| | 19 | Cast Iron - Malleable | Ferritic | | 130 | 460 | 20 | 3 | 12 | 2 | 15 | 2 | 22 | 2 | 22 | 3 |
| | 20 | | Pearlitic | | 230 | 780 | 20 | 3 | 12 | 2 | 15 | 2 | 22 | 2 | 22 | 3 |
| | 21 | Aluminum & Magnesium | Non Heat Treatable | | 60 | 210 | 70 | 6 | 42 | 5 | 51 | 5 | 70 | 5 | 70 | 6 |
| | 22 | - wrought alloy | Heat Treatable | AH | 100 | 360 | 70 | 6 | 42 | 5 | 51 | 5 | 70 | 5 | 70 | 6 |
| | 23 | Aluminum & Magnesium - cast alloy ≤12% Si | Non Heat Treatable | | 75 | 270 | 50 | 5 | 30 | 4 | 33 | 4 | 55 | 4 | 55 | 5 |
| | 24 | | Heat Treatable | AH | 90 | 320 | 50 | 5 | 30 | 4 | 33 | 4 | 55 | 4 | 55 | 5 |
| N | 25 | Al & Mg - cast alloy >12% Si | Non Heat Treatable | | 130 | 460 | 30 | 6 | 18 | 5 | 21 | 5 | - | - | - | - |
| IN | 26 | Copper & Cu alloys | Free cutting, Pb > 1% | | 110 | 390 | 25 | 5 | 15 | 4 | 18 | 4 | 40 | 4 | 40 | 5 |
| | 27 | (Brass/Bronze) | Brass (CuZn, CuSnZn) | | 90 | 320 | - | - | - | - | - | - | - | - | - | - |
| | 28 | | Bronze (CuSn) | | 100 | 360 | 50 | 6 | 30 | 5 | 33 | 5 | 70 | 5 | 70 | 6 |
| | 29 | Non-metallic - Thermosetti | ing & fiber-reinforced p | olastics | | | - | - | - | - | - | - | - | - | - | - |
| | 30 | Non-metallic - Hard rubbe | er, wood etc. | | | | - | - | - | - | - | - | - | - | - | - |
| | 31 | High temp. alloys | Fe based | Α | 200 | 680 | - | - | - | - | - | - | - | - | - | - |
| | 32 | | | AH | 280 | 950 | - | - | - | - | - | - | - | - | - | - |
| | 33 | | Ni / Co based | Α | 250 | 840 | - | - | - | - | - | - | - | - | - | - |
| | 34 | | | AH | 350 | 1180 | - | - | - | - | - | - | - | - | - | - |
| | 35 | | | С | 320 | 1080 | - | - | - | - | - | - | - | - | - | - |
| S | 36 | Titanium & Ti alloys | CP Titanium | | 400 MPa | | - | - | - | - | - | - | - | - | - | - |
| | 37.1 | , | Alpha alloys | | 860 MPa | | - | - | - | - | - | - | - | - | - | - |
| | 37.2 | | Alpha / Beta alloys | Α | 960 MPa | | - | - | - | - | - | - | - | - | - | - |
| | 37.3 | | , , | AH | 1170 MPa | | - | - | - | - | - | - | - | - | - | - |
| | 37.4 | | Beta alloys | Α | 830 MPa | | - | - | - | - | - | - | - | - | - | - |
| | 37.5 | | , , | AH | 1400 MPa | | - | - | - | - | - | - | - | - | - | - |
| | 38.1 | Hardened steel | | HT | 45 HRC | | - | - | - | - | - | - | - | - | - | - |
| | 38.2 | | | HT | 55 HRC | | - | - | - | - | - | - | - | - | - | - |
| | 39.1 | | | HT | 58 HRC | | - | - | - | - | - | - | - | - | - | - |
| Н | 39.2 | | | HT | 62 HRC | | - | - | - | - | - | - | - | - | - | - |
| | 40 | Cast Iron | Chilled | С | 400 | 1350 | _ | - | - | _ | - | - | 25 | - | 25 | 3 |
| | 41 | | 2.11100 | HT | 55 HRC | .500 | - | - | - | - | - | - | - | - | - | - |

Condition: A (Annealed), AH (Age Hardened), C (Cast),
HT (Hardened & Tempered), QT (Quenched & Tempered)
Bold = Optimal | Regular = Effective

Notes on Milling

- 1. Above values are guidelines for the size and type of cut nominated.
- 2. For long series tools, reduce speed by 40% and feed by 20%.

| | Feed Table (fz) (mm/tooth) | | | | | | | | | | | | | | | | | | | |
|------|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| - CK | | | | | | | | | | Fee | ed # | | | | | | | | | |
| Ø | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 |
| 2 | 0.001 | 0.002 | 0.002 | 0.003 | 0.004 | 0.005 | 0.006 | 0.007 | 0.008 | 0.010 | 0.011 | 0.013 | 0.014 | 0.016 | 0.018 | 0.020 | 0.022 | 0.024 | 0.026 | 0.030 |
| 3 | 0.002 | 0.003 | 0.004 | 0.005 | 0.006 | 0.008 | 0.009 | 0.010 | 0.012 | 0.014 | 0.016 | 0.018 | 0.020 | 0.023 | 0.025 | 0.028 | 0.032 | 0.034 | 0.038 | 0.042 |
| 4 | 0.004 | 0.005 | 0.006 | 0.007 | 0.009 | 0.010 | 0.012 | 0.014 | 0.016 | 0.018 | 0.021 | 0.023 | 0.026 | 0.030 | 0.032 | 0.036 | 0.040 | 0.044 | 0.045 | 0.050 |
| 5 | 0.005 | 0.006 | 0.008 | 0.009 | 0.011 | 0.013 | 0.015 | 0.017 | 0.020 | 0.023 | 0.025 | 0.030 | 0.032 | 0.036 | 0.040 | 0.044 | 0.050 | 0.055 | 0.060 | 0.065 |
| 6 | 0.006 | 0.008 | 0.009 | 0.011 | 0.013 | 0.016 | 0.018 | 0.021 | 0.024 | 0.028 | 0.030 | 0.034 | 0.038 | 0.042 | 0.045 | 0.050 | 0.055 | 0.060 | 0.070 | 0.075 |
| 8 | 0.010 | 0.012 | 0.014 | 0.017 | 0.019 | 0.022 | 0.025 | 0.028 | 0.032 | 0.036 | 0.040 | 0.045 | 0.050 | 0.055 | 0.060 | 0.065 | 0.075 | 0.080 | 0.085 | 0.095 |
| 10 | 0.013 | 0.015 | 0.018 | 0.021 | 0.024 | 0.028 | 0.032 | 0.036 | 0.040 | 0.045 | 0.050 | 0.055 | 0.060 | 0.070 | 0.075 | 0.085 | 0.090 | 0.100 | 0.11 | 0.12 |
| 12 | 0.016 | 0.019 | 0.022 | 0.026 | 0.030 | 0.034 | 0.038 | 0.044 | 0.050 | 0.055 | 0.060 | 0.065 | 0.075 | 0.080 | 0.090 | 0.100 | 0.11 | 0.12 | 0.13 | 0.14 |
| 16 | 0.020 | 0.024 | 0.028 | 0.034 | 0.038 | 0.044 | 0.050 | 0.055 | 0.060 | 0.070 | 0.080 | 0.085 | 0.095 | 0.11 | 0.12 | 0.13 | 0.14 | 0.16 | 0.17 | 0.18 |
| 20 | 0.022 | 0.028 | 0.032 | 0.038 | 0.044 | 0.050 | 0.060 | 0.065 | 0.075 | 0.085 | 0.095 | 0.11 | 0.12 | 0.13 | 0.15 | 0.16 | 0.18 | 0.19 | 0.21 | 0.23 |
| 25 | 0.025 | 0.032 | 0.038 | 0.045 | 0.055 | 0.060 | 0.070 | 0.080 | 0.090 | 0.10 | 0.12 | 0.13 | 0.15 | 0.16 | 0.18 | 0.20 | 0.22 | 0.24 | 0.26 | 0.29 |

| HSS Ti. | 192 6 Co.8 AJIN | HSS B | 113 Co.8 rt | HSS | 146 Co.8 Irt | | |
|-----------------|-----------------------|----------|-------------------|----------|--------------------|--------------|-----|
| | 30 | | 30 | | R (Long) | | |
| | _ | | | | | | |
| ' | • | | | | | | |
| | | | | | • | | |
| | | (| • | | | | |
| | .5).1 | | 05 -0.05 | | .5 25 | | |
| Vc | Feed# | Vc | Feed# | Vc | Feed# | VDIA 3323 | ISO |
| 50 | 4 | 40 | 5 | 30 | 5 | 1 | |
| 50 | 4 | 40 | 5 | 30 | 5 | 2 | |
| 50 50 | 4 | 40 40 | 5 5 | 30 30 | 5 5 | 3 | |
| 30 | 3 | 30 | 4 | 30 | 5 | 5 | |
| 50 | 4 | 40 | 5 | 30 | 5 | 6 | |
| 40 | 4 | 35 | 4 | 30 | 5 | 7 | P |
| 30 | 3 | 30 | 4 | 30 | 5 | 8 | |
| 25 30 | 3 3 | 30 | - 4 | - | - | 9 | |
| 25 | 3 | - | - | - | - | 11 | |
| 12 | 2 | - | - | - | - | 12 | |
| 25 | 3 | - | - | - | - | 13 | |
| 20 | 3 | 20 | 4 | - | - | 14.1 | |
| 15 12 | 1 2 | 15 - | 2 | - | - | 14.2 14.3 | M |
| 40 | 3 | 40 | 4 | 40 | 8 | 15 | |
| 30 | 2 | 30 | 3 | - | - | 16 | |
| - | - | 25 | 2 | 10 | 8 | 17 | K |
| - | - | 25 | 2 | - | - | 18 | ^ |
| - | - | 25 25 | 2 | 10 | 8 | 19 20 | |
| 75 | 5 | 80 | 6 | 80 | 9 | 21 | |
| 75 | 5 | 80 | 6 | 80 | 9 | 22 | |
| 60 | 4 | 55 | 5 | 55 | 8 | 23 | |
| 60 | 4 | 55 | 5 | 55 | 8 | 24 | |
| 50 40 | 4 | 50 25 | 5 5 | - 25 | - 6 | 25 26 | N |
| - | - | - | - | - | - | 27 | |
| 75 | 5 | 50 | 6 | 40 | 6 | 28 | |
| - | - | - | - | - | - | 29 | |
| - | - | - | - | - | - | 30 | |
| - | - | - | - | - | - | 32 | |
| - | - | - | - | - | - | 33 | |
| - | - | - | | - | - | 34 | |
| - | - | - | - | - | - | 35 | s |
| - | - | - | - | - | - | 36 37.1 | , |
| - | - | - | - | - | - | 37.2 | |
| - | - | - | - | - | - | 37.3 | |
| - | - | - | - | - | - | 37.4 | |
| - | - | - | - | - | - | 37.5 | |
| - | - | - | - | - | - | 38.1 38.2 | |
| - | - | - | - | - | - | 39.1 | |
| - | - | - | - | - | - | 39.2 40 | Н |
| - | 3 | - | | | | | |
| - | | - | - | - | - | 41 | |

Application Guide Troubleshooting - Drills



| Co | ode | Proble | em | | | | | | | | | | | | |
|----|-----|----------|------------|----------|----|---|---|---|---|--|--|--|--|--|--|
| , | 1 | Breaki | ng of dri | I | | | | | | | | | | | |
| : | 2 | Outer | corner b | reaks do | wn | | | | | | | | | | |
| ; | 3 | Cutting | g edges | chip | | | | | | | | | | | |
| | 4 | Drill sp | lits up c | entre | | | | | | | | | | | |
| | 5 | Drill wi | ll not ent | ter work | | | | | | | | | | | |
| (| 6 | Hole ro | ough | | | | | | | | | | | | |
| | 7 | Hole o | versize | | | | | | | | | | | | |
| 1 | 8 | Tang b | reaks | | | | | | | | | | | | |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | Possible Reason | Solution | | | | | | |
| • | | | | • | • | | | Dull point | Sharpen | | | | | | |
| • | | | | | | | | Drill has front taper due to wearing | Sharpen | | | | | | |
| • | | | • | • | | | | Insufficient lip clearance on point | Grind correctly | | | | | | |
| • | | • | | | | | | Lip clearance too great | Regrind to correct clearance angle | | | | | | |
| • | | | | | | | | Drill in incorrectly point ground | Regrind correctly | | | | | | |
| • | • | | | | | | | Flutes clogged with chips Remove drill from hole and to clear flutes | | | | | | | |
| • | | | | | | | | Spring or backlash in drill press, fixture or work | Check each item for rigidity and alignment | | | | | | |
| • | | • | • | | • | | | Feed too heavy | Reduce Feed | | | | | | |
| | • | | | | | | | Cutting speed too high | Reduce speed | | | | | | |
| | • | | | | • | | | Dry cutting, no lubricant at cutting edges | Apply cutting fluid | | | | | | |
| | | | | • | | | | Drill web (core) diameter too big | Thin web to original size | | | | | | |
| | | | | | • | | | Fixture/Clamping not rigid | Secure job firmly | | | | | | |
| | | | | | | • | | Unequal angle or uneven length of cutting edges | Regrind to same lip lengths and angles | | | | | | |
| | | | | | | • | | Spindle run-out/Loose spindle | Check machine | | | | | | |
| | | | | | | | • | Bad fit between shank taper & socket. The drive & alignment is controlled by the taper fit | Remove dirt, nicks or burrs, or replace worn socket | | | | | | |

Application Guide Troubleshooting - Taps



| Code | Probl | em | | | | | |
|------|--------|------------|------------|--------------------------------|--|--|---|
| 1 | Threa | d is overs | size | | | | |
| 2 | Axialı | niscuttir | ng of thre | ad | | | |
| 3 | Threa | d is unde | rsize | | | | |
| 4 | Threa | d has bel | Imouthe | d entry | | | |
| 5 | Threa | d surface | e is rough | n and und | clean | | |
| 6 | Low to | ool life | | | | | |
| 7 | Partia | l or comp | olete tap | breakag | e on FOI | RWARD or BACKWARD movement | |
| 1 2 | 3 | 4 | 5 | 6 | 7 | Possible reason | Solution |
| • | • | • | • | • | • | Wrong tap, cutting geometry of the tap is not suitable for this operation | Use correct tap for the material group. See Expert Tool Selector, at www.suttontools.com/expert-tool-selector |
| • | | | • | • | | Tap hole diameter is undersize | Tap hole diameter should be in accordance to DIN336 or respective standard. For cold forming taps, a special hole diameter is needed. |
| • | | • | | | • | Misalignment - tap hole position, or angle is not correct | a) check workpiece clamping b) check machine settings |
| • | | | | | | The axial machine spindle movement is not free and easy | a) use mechanical feed b) use tap holder with length compensation |
| • | | | | | | Cold welding on the thread flanks of the tap | a) use a new tap b) improve and check lubrication c) remove cold welding area from tap d) use tap with surface treatment or coatings |
| • | | | | | | Poor guidance of the tap because of little thread depth | a) use mechanical feed b) use tap that has better guiding characteristics |
| • | • • | | | | | Speed is too high | a) improve lubrication b) lower speed |
| • | | | • | • | | Chip clogging | a) use tap with different flute form b) use coated taps c) use tap set |
| • | | | • | • | | The lubrication wrong, additives or the coolant supply is not sufficient | Make sure that the coolant is correct and that the supply is sufficient |
| • | | | | | | Spiral fluted taps are over pressured in the initial cutting phase (retracting pulling force) | Spiral fluted taps should only be lightly pushed into the tap hole until it begins to cut. The tap holder should immediatel begin to apply tension to the tap. |
| • | | | | | | Spiral pointed taps (gun taps) are not receiving enough pressure in the initial cutting phase | Spiral pointed taps and even left hand spiral flute taps must have a stronger pressure until they begin to cut. The tap holder should immediately begin to apply pressuto the tap (pushing force) |
| • | • | | | | | Tolerance on the tap is not identical to the tolerance on the drawing or on the gauge | Use a tap which has a correct tolerance |
| | | • | | | | Wrong initial cutting pressure has been used or the machine spindle is not moving along its axis free and easy | a) use mechanical feed b) use tap holder with length compensation |
| | | | • | • | | Tap is over loaded, either from coarse pitch and/or tough material | Use set of taps |
| | | | | • | | Cold welding, material build-up (pick-up) | a) improve coolant supply, use taps with surface treatments or coatings b) check if surface treatment is correct for this application |
| | • • | | • | Hardened walls in drilled hole | a) use drill best suited to material being drilled b) use new drill or boring tool c) resharpen drilling or boring tools d) if possible, heat treatment and coatings should only be made after threading | | |
| | | | | | • | Over loading of teeth in the chamfer area | a) use a longer chamfer (check if the tap hole is blind hole or through) b) use increased number of teeth in the chamfer area by selecting tap with increased number of flutes |
| | | | | | | Tap hole chamfer is missing or wrong | Countersink tap hole chamfer with correct angle |
| | | | | | • | Tap crashed against the bottom of tap hole | Use tap holder with length compensation and over load clutch |
| | _ | | | | | | · |

Application Guide Troubleshooting - Endmills



| Co | de | Proble | em | | | | | | | Possible Reason | | |
|----|----|------------------------------------|------------|------------|--------------------------------|-----------|----------------------|---|---|---|--|--|
| 1 | 1 | Poor w | orkpiece | e finish | | | | | | Cutting edge wear, cutter radial run-out | | |
| 2 | 2 | Splinte | ering of v | vorkpiec | e edge | | | | | Unsuitable cutting conditions, unsuitable shape of cutting edge | | |
| 3 | 3 | Non-p | arallel or | uneven | surface | | | | | Low stiffness of the cutter or of the workpiece (loose) | | |
| 4 | Į. | Extren | ne flank v | wear | | | | | | | | |
| Ę | 5 | Extren | ne crater | wear | | | | | | | | |
| 6 | 6 | Breaks | and she | elling due | to thern | nal shock | (| | | Unsuitable cutting conditions, unsuitable shape of cutting edge | | |
| 7 | 7 | Forma | tion of b | uilt-up e | dges | | | | | | | |
| 8 | 3 | Poor chip clearance, chip blockage | | | | | | | | | | |
| 9 | • | Lack of Rigidity | | | | | | | | Difficult cutting conditions, clamping of the workpiece | | |
| 1 | 0 | Endmill cutter breaks | | | | | | | | Unsuitable cutting conditions, flute length of the cutter | | |
| 1 | 2 | 3 4 5 6 7 8 9 10 | | | | | 8 | 9 | 10 | Solution | | |
| • | | | | | | • | • | | | increase cutting speed | | |
| | | | | | | | | | | reduce cutting speed | | |
| | | • • | | | | | • | | | increase feed rate | | |
| • | • | • • • • • | | | | • | • | • | reduce feed rate | | | |
| • | • | • • • • | | | • | • | reduce cutting depth | | | | | |
| | | | | | | | • | • | • | change cutter diameter and cut width | | |
| • | | | • | • | | • | • | | | check use of cooling lubricant, flush swarf away | | |
| | • | • | • | • | • | • | • | • | | increase clearance angle (Radial relief) | | |
| | • | | | • | • | | | | | increase wedge angle (Rake angle) | | |
| | • | | | | | | | | | increase number of teeth | | |
| | | • | | | | | • | • | • | reduce number of teeth | | |
| | | | | | | | • | | | select larger chip space (Cutter) | | |
| • | • | • | • | | • | | | | | change shape of minor cutting edge | | |
| | | • | | | cutter - change radial run-out | | | | | | | |
| | • | • | | | | | • | • | change cutter stiffness, flute length (I/D ratio) | | | |
| | • | • | | | • | | | • | | select machine with higher power and stiffness | | |

Application Guide Troubleshooting - Reamers



| Code | Problem | | | | | | |
|------|--------------|--|--|--|--|--|--|
| 1 | Breakage | | | | | | |
| 2 | Excessive we | ar | | | | | |
| 3 | Chattering | | | | | | |
| 4 | Poor surface | finish | | | | | |
| 1 2 | 3 4 | Possible reason | Solution | | | | |
| • | • | Dirt or burrs in spindle or socket in which reamer is held | clean spindle | | | | |
| • | | Misalignment of two or more parts of the set-up. This condition can cause a bell-mouthed hole | align holes or use bridge style reamer | | | | |
| • | • | Too fast or too slow speeds | adjust | | | | |
| • | • | Too much or too little feed | adjust | | | | |
| • | | Wrong type of coolant | refer to lubricant supplier's literature | | | | |
| • | | No lubricant between guide bushing and reamer | apply | | | | |
| • | • | Lack of lubricant | increase | | | | |
| • | | Bottoming in blind holes | reduce depth travel of reamer | | | | |
| | • | Lack of sufficient stock to ream | drill smaller hole | | | | |
| • | • | Too much stock to ream | drill larger hole | | | | |
| • | • | Entering work too fast | slow down the approach feed, until all cutting edges are located in the hole | | | | |
| • | • | Badly drilled holes – too rough, tapered or bell-mouthed. Bell- mouthed holes may cause the reamer to wedge rather than cut | replace drill | | | | |
| | • | Oversize or undersize bushings | use suitable bush | | | | |
| • | • | Lack of rigidity in machine or work holder | improve rigidity | | | | |
| • | • | Improperly designed reamer for the job | use a different reamer | | | | |

| Trade Name | Coating | Coating Structure | Micro- hardness | Coeff. of Friction vs Steel | Thermal Stability | Colour | Application & Benefits | | |
|------------------------|----------------------------------|----------------------|--------------------|-----------------------------------|----------------------|---------------|--|--|--|
| Alcrona (AlCrN) | Aluminium Chromium Nitride | Mono Layer | 3200 HV | 0.35 | up to 2012°F | Blue - Grey | Low alloy steels and high tensile steels Hardened steels up to 54 HRC Ideal for carbide tools | | |
| Aldura | TiAIN + AlCrN | Multi Layer | 3300 HV | <0.4 | >1100°C | Blue - Grey | High speed machining Suitable for minimum quantity lubrication (MQL) and dry machining Machining of hardened steels (>60HRC) Ideal for carbide tools | | |
| AlNova | Alcrona based | Multi Layer | 3200 HV | 0.35 | >1100°C | Light Grey | Even high thermal stresses hardly effect the superior hardness of the coating Its high hot hardness results in excellent abrasion resistance even at high cutting speeds | | |
| Blu | Steam Oxide | - | - | 0.8 - 1.0 | - | Blue - Black | For ferrous metals Prevents chip build-up on the cutting edges, especially in low carbon steels Oxide layer protects surface Good carrier of lubricants | | |
| Brt | - | - | - | 0.8 - 1.0 | - | - | For general purpose applications | | |
| CrN | Chromium Nitride | Gradient Coating | 1750 HV | 0.5 | up to 1292°F | Silver - Grey | Low internal stress of coating results in excellent adhesion under high loads | | |
| Futura Nano (TiAIN) | Titanium Aluminium Nitride | Nano Layer | 3300 HV | 0.3 - 0.35 | up to 1652°F | Violet - Grey | Abrasive materials - cast iron and heat treated steel Difficult to machine materials, such as stainless steel | | |
| Hardlube | TiAIN + WC/C | Nano Layer | 3000 HV | 0.15-0.20 | up to 1472°F | Dark Grey | Excellent friction and lubricating properties of the coating provide optimal chip flow Tapping and drilling of hard to machine materials Suitable for minimum quantity lubrication (MQL) and dry machining | | |
| Helica | Alcrona based | Multi Layer | 3000 HV | 0.25 | up to 1100°C | Copper | Longer tool life Higher cutting speeds and feeds Superb chip evacuation Greater number of regrinds Improved drill hole quality Excellent performance in abrasive material | | |
| Ni | Plasma Nitride | - | - | 0.8 - 1.0 | - | - | Increases surface hardness Better lubricant carrying properties Abrasive materials - cast iron and Aluminium alloys | | |
| TiN | Titanium Nitride | Mono Layer | 2300 HV | 0.4 | up to 1112°F | Gold - Yellow | General purpose use Wide range of materials 3 to 8 times longer tool life than uncoated tools Higher tool speeds and feeds than uncoated tools | | |
| TiCN | Titanium Carbonitride | Gradient Coating | 3000 HV | 0.4 | up to 752°F | Blue - Grey | High performance applications Difficult to machine materials Abrasive materials - cast iron and Aluminium alloys Adhesive materials - copper and copper based alloys | | |
| TiSiN | TiSi based | Multi Layer | 3600 HV | 0.3 | <1200°C | Copper | Suitable for high speed (wet / dry) and hard machining for difficult materials above 52 HRC. Suitable for high speed machining with hardened steels above 60 HRC to maximum of 63 HRC Vc & Vf = +50% | | |

Latest advances in thin film coatings to optimise your machining application



| Abbreviations | Туре | Application | Description |
|---------------|--|---|---|
| HSS | Conventional high speed steel | Standard tool material for most common applications | Used for the manufacturing of cutting tools such as twist drills, endmills and taps. |
| HSS Co | 5% cobalt grade of high speed steel | High-heat resistance, especially suited for roughing or when coolant insufficient | Cobalt alloyed, tungsten-molybdenum high speed steel possessing high hardness, excellent cutting properties, high-red hardness and good toughness. |
| HSSE Co 8% | 8% cobalt grade of high speed steel | Increased heat resistance and hardness, suitable for difficult-to-machine materials | Available for applications that require a strong resistance to softening at elevated cutting temperatures. The ability of the steel to maintain its "red-hot hardness" is provided by the addition of cobalt. The high hot hardness is required for machining difficult materials such as nickel-base, titanium and highly alloyed steel. |
| HSSE | Premium grade of high speed steel | Wide range of machine taps | Vanadium grade gives high wear resistance and toughness for most tapping applications. |
| PM-HSSE V3 | Powdered metallurgy - vanadium grade of high speed steel | Materials with hardness up to 40 HRC Difficult-to-machine materials eg. stainless steels | PM-HSS V3 for higher performance tools, incorporates very fine and uniform grain structure allowing a high hardness to be achieved, whilst maintaining good toughness. |
| PM-HSS Co | Powdered metallurgy - 8% Cobalt grade of high speed steel | Materials with hardness up to 45 HRC | The addition of cobalt provides this material with the ability to maintain its strength and hardness level when exposed to extremely high cutting temperatures. This makes PM-HSS Co suitable for heavy duty tapping, in materials such as high alloyed steels to non-ferrous metals like Ni-base alloys & Ti-alloys. |
| SPM | Powdered metallurgy - 11% Cobalt grade of high speed steel | Special applications, requiring very high edge hardness. Cutting tools with the appropriate geometry can be applied to workpiece materials with hardness up to 55 HRC | An excellent bridge material between high speed steel and carbide. SPM offers very high red hardness, wear resistance and the highest compressive strength of any high speed steel. |
| VHM | Sub-micron grade of solid Carbide (ISO K15-K30) | Tapping hardened steel | Ultra fine grain type (0.8µm) with maximum toughness & high hardness, therefore especially recommended for rotating tools to machine hardened parts. |
| VHM | Sub-micron grade of solid Carbide (ISO K40) | Sutton standard grade for endmills & drills | Ultra fine grain type (0.6µm) offers the ideal combination of hardness & toughness for high performance drilling & general milling applications |
| VHM-ULTRA | Sub-micron grade of solid Carbide (ISO K40-K50) | High performance grade for endmills | Ultra fine grain type (0.5µm) offers the best wear resistance for high performance milling applications. |

Computer controlled vacuum heat treatment ensures consistent high quality



| Metric | Imperial | Inch | Gauge | Metric | Imperial | Inch | Gauge | Metric | Imperial | Inch | Gauge |
|--------|----------|--------|------------|--------|----------|--------|-------|----------------|----------|------------------|-------|
| 0.010 | | 0.0004 | | 1.092 | • | 0.0430 | 57 | 3.800 | • | 0.1496 | |
| 0.100 | | 0.0039 | | 1.181 | | 0.0465 | 56 | 3.861 | | 0.1520 | 24 |
| 0.150 | | 0.0059 | 97 | 1.191 | 3/64 | 0.0469 | 00 | 3.900 | | 0.1535 | |
| 0.160 | | 0.0063 | 96 | 1.321 | 0,04 | 0.0520 | 55 | 3.912 | | 0.1540 | 23 |
| 0.170 | | 0.0067 | 95 | 1.397 | | 0.0550 | 54 | 3.969 | 5/32 | 0.1563 | LU |
| 0.180 | | 0.0071 | 94 | 1.500 | | 0.0591 | • | 3.988 | 0,02 | 0.1570 | 22 |
| 0.190 | | 0.0075 | 93 | 1.511 | | 0.0595 | 53 | 4.000 | | 0.1575 | |
| 0.200 | | 0.0079 | 92 | 1.588 | 1/16 | 0.0625 | 00 | 4.039 | | 0.1590 | 21 |
| 0.210 | | 0.0083 | 91 | 1.613 | 2,20 | 0.0635 | 52 | 4.089 | | 0.1610 | 20 |
| 0.220 | | 0.0087 | 90 | 1.702 | | 0.0670 | 51 | 4.100 | | 0.1614 | |
| 0.230 | | 0.0091 | 89 | 1.778 | | 0.0700 | 50 | 4.200 | | 0.1654 | |
| 0.240 | | 0.0094 | 88 | 1.854 | | 0.0730 | 49 | 4.216 | | 0.1660 | 19 |
| 0.254 | | 0.0100 | 87 | 1.900 | | 0.0730 | 43 | 4.300 | | 0.1693 | 10 |
| 0.270 | | 0.0106 | 86 | 1.930 | | 0.0740 | 48 | 4.305 | | 0.1695 | 18 |
| 0.280 | | 0.0110 | 85 | 1.984 | 5/64 | 0.0781 | 40 | 4.366 | 11/64 | 0.1719 | 10 |
| 0.290 | | 0.0114 | 84 | 1.994 | 0,04 | 0.0785 | 47 | 4.394 | 11/04 | 0.1710 | 17 |
| 0.300 | | 0.0114 | 04 | 2.000 | | 0.0787 | 47 | 4.400 | | 0.1732 | 1, |
| 0.305 | | 0.0110 | 83 | 2.057 | | 0.0810 | 46 | 4.496 | | 0.1770 | 16 |
| 0.317 | | 0.0125 | 82 | 2.083 | | 0.0820 | 45 | 4.500 | | 0.1770 | 10 |
| 0.330 | | 0.0123 | 81 | 2.184 | | 0.0860 | 44 | 4.572 | | 0.1800 | 15 |
| 0.343 | | 0.0135 | 80 | 2.261 | | 0.0890 | 43 | 4.600 | | 0.1811 | 10 |
| 0.368 | | 0.0135 | 79 | 2.375 | | 0.0935 | 42 | 4.623 | | 0.1820 | 14 |
| 0.397 | 1/64 | 0.0143 | 73 | 2.381 | 3/32 | 0.0938 | 76 | | | | 13 |
| 0.400 | 1/04 | 0.0150 | | 2.438 | 3/32 | 0.0960 | 41 | 4.700 4.762 | 3/16 | 0.1850 0.1875 | 13 |
| 0.406 | | 0.0137 | 78 | 2.489 | | 0.0980 | 40 | 4.800 | 3/10 | 0.1873 | 12 |
| 0.400 | | 0.0180 | 77 | 2.500 | | 0.0984 | 40 | 4.851 | | 0.1030 | 11 |
| 0.437 | | 0.0180 | 11 | 2.527 | | 0.0984 | 39 | 4.900 | | 0.1910 | 11 |
| 0.508 | | 0.0197 | 76 | 2.578 | | 0.1015 | 38 | 4.900 | | 0.1929 | 10 |
| 0.533 | | 0.0200 | 76 75 | 2.642 | | 0.1013 | 37 | 4.913 | | 0.1933 | 9 |
| 0.572 | | 0.0210 | 74 | 2.705 | | 0.1040 | 36 | 5.000 | | 0.1969 | 9 |
| 0.600 | | 0.0225 | 74 | 2.778 | 7/64 | 0.1003 | 30 | 5.055 | | 0.1909 | 8 |
| 0.610 | | 0.0230 | 73 | 2.778 | 7/04 | 0.1100 | 35 | 5.100 | | 0.2008 | |
| 0.635 | | 0.0240 | 73 72 | 2.794 | | 0.1100 | 34 | 5.105 | | 0.2008 | 7 |
| 0.660 | | 0.0260 | 71 | 2.870 | | 0.1110 | 33 | 5.159 | 13/64 | 0.2010 | |
| 0.700 | | 0.0276 | /- | 2.946 | | 0.1160 | 32 | 5.182 | 13/04 | 0.2040 | 6 |
| 0.711 | | 0.0280 | 70 | 3.000 | | 0.1181 | J. | 5.200 | | 0.2047 | J |
| 0.711 | | 0.0292 | 69 | 3.048 | | 0.1200 | 31 | 5.220 | | 0.2055 | 5 |
| 0.742 | | 0.0232 | 68 | 3.100 | | 0.1200 | O. | 5.300 | | 0.2033 | |
| 0.794 | 1/32 | 0.0313 | | 3.175 | 1/8 | 0.1250 | | 5.309 | | 0.2090 | 4 |
| 0.800 | _, ~_ | 0.0315 | | 3.200 | _, 0 | 0.1260 | | 5.400 | | 0.2126 | |
| 0.813 | | 0.0320 | 67 | 3.264 | | 0.1285 | 30 | 5.410 | | 0.2120 | 3 |
| 0.838 | | 0.0330 | 66 | 3.300 | | 0.1299 | | 5.500 | | 0.2165 | |
| 0.889 | | 0.0350 | 65 | 3.400 | | 0.1233 | | 5.556 | 7/32 | 0.2188 | |
| 0.900 | | 0.0354 | | 3.454 | | 0.1360 | 29 | 5.600 | -, | 0.2205 | |
| 0.914 | | 0.0360 | 64 | 3.500 | | 0.1378 | | 5.613 | | 0.2210 | 2 |
| 0.940 | | 0.0370 | 63 | 3.569 | | 0.1405 | 28 | 5.700 | | 0.2244 | _ |
| 0.965 | | 0.0380 | 62 | 3.572 | 9/64 | 0.1406 | | 5.791 | | 0.2280 | 1 |
| 0.991 | | 0.0390 | 61 | 3.600 | 5,01 | 0.1417 | | 5.800 | | 0.2283 | |
| 1.000 | | 0.0394 | ~ - | 3.658 | | 0.1440 | 27 | 5.900 | | 0.2323 | |
| 1.016 | | 0.0400 | 60 | 3.700 | | 0.1457 | | 5.944 | | 0.2340 | Α |
| 1.041 | | 0.0410 | 59 | 3.734 | | 0.1470 | 26 | 5.953 | 15/64 | 0.2344 | -1 |
| 1.067 | | 0.0420 | 58 | 3.797 | | 0.1495 | 25 | 6.000 | 20,04 | 0.2362 | |
| 1.007 | | 0.0420 | | 0.707 | | 0.1700 | LU | 3.000 | | 0.2002 | |

| Metric | Imperial | Inch | Gauge | Metric | Imperial | Inch | Gauge | Metric | Imperial | Inch | Gauge |
|--------|----------|--------|-------|--------|----------|--------|-------|--------|----------|--------|-------|
| 6.045 | | 0.2380 | В | 8.900 | | 0.3504 | | 15.500 | | 0.6102 | |
| 6.100 | | 0.2402 | | 9.000 | | 0.3543 | | 15.875 | 5/8 | 0.6250 | |
| 6.147 | | 0.2420 | С | 9.093 | | 0.3580 | т | 16.000 | -,- | 0.6299 | |
| 6.200 | | 0.2441 | | 9.100 | | 0.3583 | | 16.272 | 41/64 | 0.6406 | |
| 6.248 | | 0.2460 | D | 9.128 | 23/64 | 0.3594 | | 16.500 | • | 0.6496 | |
| 6.300 | | 0.2480 | | 9.200 | | 0.3622 | | 16.669 | 21/32 | 0.6563 | |
| 6.350 | 1/4 | 0.2500 | E | 9.300 | | 0.3661 | | 17.000 | • - | 0.6693 | |
| 6.400 | • | 0.2520 | | 9.347 | | 0.3680 | U | 17.066 | 43/64 | 0.6719 | |
| 6.500 | | 0.2559 | | 9.400 | | 0.3701 | | 17.462 | 11/16 | 0.6875 | |
| 6.528 | | 0.2570 | F | 9.500 | | 0.3740 | | 17.500 | • | 0.6890 | |
| 6.600 | | 0.2598 | | 9.525 | 3/8 | 0.3750 | | 17.859 | 45/64 | 0.7031 | |
| 6.629 | | 0.2610 | G | 9.576 | | 0.3770 | V | 18.000 | | 0.7087 | |
| 6.700 | | 0.2638 | | 9.600 | | 0.3780 | | 18.256 | 23/32 | 0.7188 | |
| 6.747 | 17/64 | 0.2656 | | 9.700 | | 0.3819 | | 18.500 | - | 0.7283 | |
| 6.756 | | 0.2660 | н | 9.800 | | 0.3858 | | 18.653 | 47/64 | 0.7344 | |
| 6.800 | | 0.2677 | | 9.804 | | 0.3860 | W | 19.000 | | 0.7480 | |
| 6.900 | | 0.2717 | | 9.900 | | 0.3898 | | 19.050 | 3/4 | 0.7500 | |
| 6.909 | | 0.2720 | ı | 9.922 | 25/64 | 0.3906 | | 19.447 | 49/64 | 0.7656 | |
| 7.000 | | 0.2756 | | 10.000 | | 0.3937 | | 19.500 | | 0.7677 | |
| 7.036 | | 0.2770 | J | 10.084 | | 0.3970 | X | 19.844 | 25/32 | 0.7813 | |
| 7.100 | | 0.2795 | | 10.200 | | 0.4016 | | 20.000 | | 0.7874 | |
| 7.137 | | 0.2810 | K | 10.262 | | 0.4040 | Y | 20.241 | 51/64 | 0.7969 | |
| 7.144 | 9/32 | 0.2813 | | 10.319 | 13/32 | 0.4063 | | 20.500 | | 0.8071 | |
| 7.200 | | 0.2835 | | 10.490 | | 0.4130 | Z | 20.638 | 13/16 | 0.8125 | |
| 7.300 | | 0.2874 | | 10.500 | | 0.4134 | | 21.000 | | 0.8268 | |
| 7.366 | | 0.2900 | L | 10.716 | 27/64 | 0.4219 | | 21.034 | 53/64 | 0.8281 | |
| 7.400 | | 0.2913 | | 10.800 | | 0.4252 | | 21.431 | 27/32 | 0.8438 | |
| 7.493 | | 0.2950 | M | 11.000 | | 0.4331 | | 21.500 | | 0.8465 | |
| 7.500 | | 0.2953 | | 11.112 | 7/16 | 0.4375 | | 21.828 | 55/64 | 0.8594 | |
| 7.541 | 19/64 | 0.2969 | | 11.200 | | 0.4409 | | 22.000 | | 0.8661 | |
| 7.600 | | 0.2992 | | 11.500 | | 0.4528 | | 22.225 | 7/8 | 0.8750 | |
| 7.671 | | 0.3020 | N | 11.509 | 29/64 | 0.4531 | | 22.500 | | 0.8858 | |
| 7.700 | | 0.3031 | | 11.800 | | 0.4646 | | 22.622 | 57/64 | 0.8906 | |
| 7.800 | | 0.3071 | | 11.906 | 15/32 | 0.4688 | | 23.000 | | 0.9055 | |
| 7.900 | | 0.3110 | | 12.000 | | 0.4724 | | 23.019 | 29/32 | 0.9063 | |
| 7.938 | 5/16 | 0.3125 | | 12.200 | | 0.4803 | | 23.416 | 59/64 | 0.9219 | |
| 8.000 | | 0.3150 | | 12.303 | 31/64 | 0.4844 | | 23.500 | | 0.9252 | |
| 8.026 | | 0.3160 | 0 | 12.500 | | 0.4921 | | 23.812 | 15/16 | 0.9375 | |
| 8.100 | | 0.3189 | | 12.700 | 1/2 | 0.5000 | | 24.000 | | 0.9449 | |
| 8.200 | | 0.3228 | | 12.800 | | 0.5039 | | 24.209 | 61/64 | 0.9531 | |
| 8.204 | | 0.3230 | Р | 13.000 | | 0.5118 | | 24.500 | | 0.9646 | |
| 8.300 | | 0.3268 | | 13.097 | 33/64 | 0.5156 | | 24.606 | 31/32 | 0.9688 | |
| 8.334 | 21/64 | 0.3281 | | 13.494 | 17/32 | 0.5313 | | 25.000 | | 0.9843 | |
| 8.400 | | 0.3307 | | 13.500 | | 0.5315 | | 25.003 | 63/64 | 0.9844 | |
| 8.433 | | 0.3320 | Q | 13.891 | 35/64 | 0.5469 | | 25.400 | 1 | 1.0000 | |
| 8.500 | | 0.3346 | | 14.000 | | 0.5512 | | | | | |
| 8.600 | | 0.3386 | | 14.288 | 9/16 | 0.5625 | | | | | |
| 8.611 | | 0.3390 | R | 14.500 | | 0.5709 | | | | | |
| 8.700 | | 0.3425 | | 14.684 | 37/64 | 0.5781 | | | | | |
| 8.731 | 11/32 | 0.3438 | | 15.000 | | 0.5906 | | | | | |
| 8.800 | | 0.3465 | | 15.081 | 19/32 | 0.5938 | | | | | |
| 8.839 | | 0.3480 | S | 15.478 | 39/64 | 0.6094 | | | | | |

Tensile Strength vs Hardness (≈)

| | Tensile Strength | Hardness | | | |
|-------|------------------|------------------------|--------------|----------------------|--|
| N/mm² | Kg/mm² | Tons/Inch ² | Brinell [HB] | Rockwell [HRC (HRB)] | |
| 400 | 40.8 | 26.0 | 119 | 69 HRB | |
| 450 | 45.9 | 29.0 | 133 | 75 HRB | |
| 500 | 50.1 | 32.4 | 149 | 81 HRB | |
| 550 | 56.0 | 35.6 | 163 | 85.5 HRB | |
| 600 | 61.0 | 38.9 | 178 | 89 HRB | |
| 650 | 66.2 | 42.1 | 193 | 92 HRB | |
| 700 | 71.4 | 45.3 | 208 | 95 HRB | |
| 750 | 76.5 | 48.5 | 221 | 97 HRB | |
| 800 | 81.6 | 51.8 | 238 | 22 HRC | |
| 850 | 86.7 | 55.1 | 252 | 25 HRC | |
| 900 | 91.8 | 58.3 | 266 | 27 HRC | |
| 1000 | 102.0 | 64.7 | 296 | 31 HRC | |
| 1100 | 112.2 | 71.2 | 325 | 35 HRC | |
| 1200 | 122.4 | 77.7 | 354 | 38 HRC | |
| 1300 | 132.6 | 84.1 | 383 | 41 HRC | |
| 1400 | 142.8 | 90.5 | 408 | 44 HRC | |
| 1500 | 152.9 | 97.0 | 444 | 47 HRC | |
| 1600 | 163.1 | 103.5 | 461 | 49 HRC | |
| 1700 | 173.3 | 109.9 | 477 | 50 HRC | |
| 1800 | 183.5 | 116.4 | 514 | 52 HRC | |
| 1900 | 193.7 | 122.9 | 549 | 54 HRC | |
| 2000 | 203.9 | 129.3 | 584 | 56 HRC | |
| 2100 | 214.1 | 135.8 | 607 | 57 HRC | |
| 2200 | 224.3 | 142.2 | 622 | 58 HRC | |
| 2300 | 233.1 | 148.7 | 653 | 60 HRC | |

Conversion of values depends on the actual alloy content; this chart therefore indicates a general conversion only.

Manufacturing Tolerances

| Nominal | | Tolerance Grade in Microns | | | | | | | | 1 Micron = 0.001mm | | | | |
|----------------------------|------------------------|----------------------------|-----|-----|-----|-----|-----|------|------|--------------------|-----|-----|------|-----|
| Diameter in mm above | up to and including | e8 | h5 | h6 | h7 | h8 | h9 | h10 | js12 | js14 | k8 | k9 | k10 | m7 |
| 0 | | -14 | 0 | 0 | 0 | 0 | 0 | 0 | +50 | +125 | +14 | +25 | +40 | +12 |
| 0 | 3 | -18 | -4 | -6 | -10 | -14 | -25 | -40 | -50 | -125 | 0 | 0 | 0 | +2 |
| 0 | | -20 | 0 | 0 | 0 | 0 | 0 | 0 | +60 | +150 | +18 | +30 | +48 | +16 |
| 3 | 6 | -38 | -5 | -8 | -12 | -18 | -30 | -48 | -60 | -150 | 0 | 0 | 0 | +4 |
| 0 | 40 | -25 | 0 | 0 | 0 | 0 | 0 | 0 | +75 | +180 | +22 | +36 | +58 | +21 |
| 6 | 10 | -47 | -6 | -9 | -15 | -22 | -36 | -58 | -75 | -180 | 0 | 0 | 0 | +6 |
| 10 | 40 | -32 | 0 | 0 | 0 | 0 | 0 | 0 | +90 | +215 | +27 | +43 | +70 | +25 |
| 10 | 18 | -59 | -8 | -11 | -18 | -27 | -43 | -70 | -90 | -215 | 0 | 0 | 0 | +7 |
| 10 | 00 | -40 | 0 | 0 | 0 | 0 | 0 | 0 | +105 | +260 | +33 | +52 | +84 | +29 |
| 18 | 30 | -73 | -9 | -13 | -21 | -33 | -52 | -84 | -105 | -260 | 0 | 0 | 0 | +8 |
| 00 | 50 | -50 | 0 | 0 | 0 | 0 | 0 | 0 | +125 | +310 | +39 | +62 | +100 | +34 |
| 30 | 50 | -89 | -11 | -16 | -25 | -39 | -62 | -100 | -125 | -310 | 0 | 0 | 0 | +9 |
| Γ0 | 00 | -60 | 0 | 0 | 0 | 0 | 0 | 0 | +150 | +370 | +46 | +74 | +120 | +41 |
| 50 | 80 | -106 | -13 | -19 | -30 | -46 | -74 | -120 | -150 | -370 | 0 | 0 | 0 | +11 |
| 00 | 100 | -72 | 0 | 0 | 0 | 0 | 0 | 0 | +175 | +435 | +54 | +87 | +140 | +48 |
| 80 | 120 | -126 | -15 | -22 | -35 | -54 | -87 | -140 | -175 | -435 | 0 | 0 | 0 | +13 |

Conversion: 1 micron equals .00004 inches

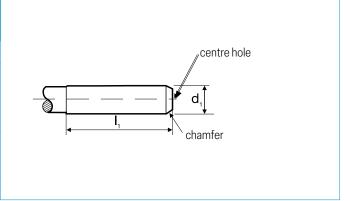
High Speed Steel Straight Shanks

DIN 1835

Form A (plain)

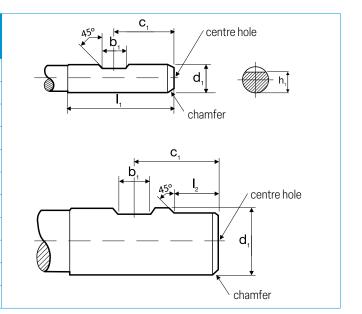
| d _ı h6 | l, +2 -0 |
|----------------------|----------------|
| 3 | 28 |
| 4 | 28 |
| 5 | 28 |
| 6 | 36 |
| 8 | 36 |
| 10 | 40 |
| 12 | 45 |

| d, h6 | l ₁ +2 -0 |
|----------|----------------------------|
| 16 | 48 |
| 20 | 50 |
| 25 | 56 |
| 32 | 60 |
| 40 | 70 |
| 50 | 80 |
| 63 | 90 |



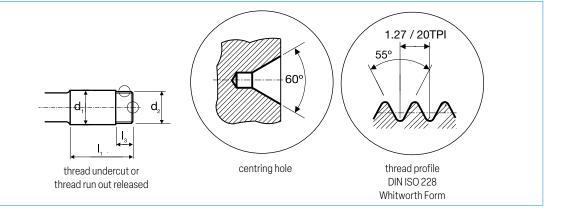
Form B (with drive flat)

| d _ı h6 | b ₁ +0.05 -0 | c ₁ 0 -1 | h _i h13 | l ₁ +2 -0 | l ₂ +1 -0 | | | | | |
|----------------------|-------------------------------|---------------------------|-----------------------|----------------------------|----------------------------|--|--|--|--|--|
| 6 | 4.2 | 18 | 4.8 | 36 | - | | | | | |
| 8 | 5.5 | 18 | 6.6 | 36 | - | | | | | |
| 10 | 7 | 20 | 8.4 | 40 | - | | | | | |
| 12 | 8 | 22.5 | 10.4 | 45 | - | | | | | |
| 16 | 10 | 24 | 14.2 | 48 | - | | | | | |
| 20 | 11 | 25 | 18.2 | 50 | - | | | | | |
| 25 | 12 | 32 | 23 | 56 | 17 | | | | | |
| 32 | 14 | 36 | 30 | 60 | 19 | | | | | |
| 40 | 14 | 40 | 38 | 70 | 19 | | | | | |
| 50 | 18 | 45 | 47.8 | 80 | 23 | | | | | |
| 63 | 18 | 50 | 60.8 | 90 | 23 | | | | | |



Form D (screwed shank)

| d ₁ | l, +2 -0 | l₃ +1 -0 | d ₂ |
|----------------|----------------|----------------|----------------|
| 6 | 36 | 10 | 5.9 |
| 10 | 40 | 10 | 9.9 |
| 12 | 45 | 10 | 11.9 |
| 16 | 48 | 10 | 15.9 |
| 20 | 50 | 15 | 19.9 |
| 25 | 56 | 15 | 24.9 |
| 32 | 60 | 15 | 31.9 |



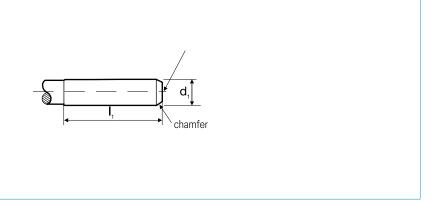
Carbide Straight Shanks

Form HA (plain)

| d ₁ h6 | l, +2 -0 |
|----------------------|----------------|
| 2 | 28 |
| 3 | 28 |
| 4 | 28 |
| 5 | 28 |
| 6 | 36 |
| 8 | 36 |
| 10 | 40 |

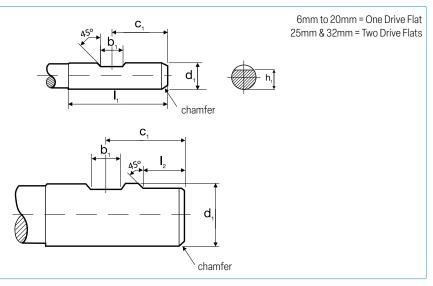
DIN6535

| l, +2 -0 |
|----------------|
| -0 |
| 45 |
| 45 |
| 48 |
| 48 |
| 50 |
| 56 |
| 60 |
| |
| |



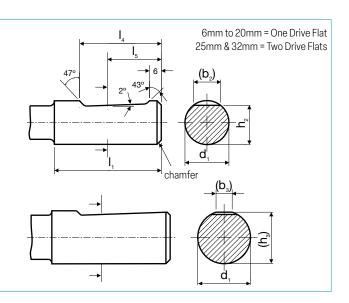
Form HB (with drive flat)

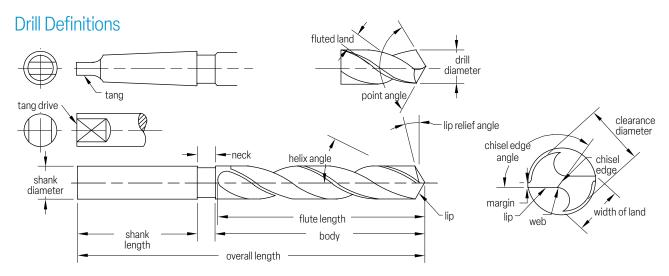
| d ₁ | b ₁ +0.05 -0 | C ₁ 0 -1 | h _i h11 | l ₁ +2 -0 | l ₂ +1 -0 |
|----------------|-------------------------------|---------------------------|-----------------------|----------------------------|----------------------------|
| 6 | 4.2 | 18 | 5.1 | 36 | - |
| 8 | 5.5 | 18 | 6.9 | 36 | - |
| 10 | 7 | 20 | 8.5 | 40 | - |
| 12 | 8 | 22.5 | 10.4 | 45 | - |
| 14 | 8 | 22.5 | 12.7 | 45 | - |
| 16 | 10 | 24 | 14.2 | 48 | - |
| 18 | 10 | 24 | 16.2 | 48 | - |
| 20 | 11 | 25 | 18.2 | 50 | - |
| 25 | 12 | 32 | 23 | 56 | 17 |
| 32 | 14 | 36 | 30 | 60 | 19 |



Form HE (with whistle notch flat)

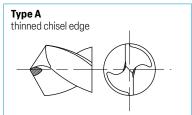
| d ₁ | b ₂ | b ₃ | h ₂ | h ₃ | l, +2 | I ₄ 0 | l ₅ |
|----------------|----------------|----------------|----------------|----------------|----------|---------------------|----------------|
| h6 | | | h11 | | 0 | -1 | |
| 6 | 4.3 | - | 5.1 | - | 36 | 25 | 18 |
| 8 | 5.5 | - | 6.9 | - | 36 | 25 | 18 |
| 10 | 7.1 | - | 8.5 | - | 40 | 28 | 20 |
| 12 | 8.2 | - | 10.4 | - | 45 | 33 | 22.5 |
| 14 | 8.1 | - | 12.7 | - | 45 | 33 | 22.5 |
| 16 | 10.1 | - | 14.2 | - | 48 | 36 | 24 |
| 18 | 10.8 | - | 16.2 | - | 48 | 36 | 24 |
| 20 | 11.4 | - | 18.2 | - | 50 | 38 | 25 |
| 25 | 13.6 | 9.3 | 23 | 24.1 | 56 | 44 | 32 |
| 32 | 15.5 | 9.3 | 30 | 31.2 | 60 | 48 | 35 |

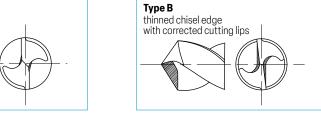


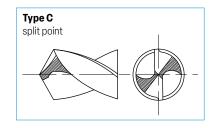


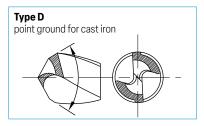
^{*}Drills manufactured to ANSI B94-11. The overall length and flute length are measured to the corner of the outer lip.

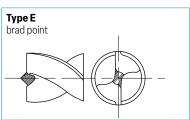
Drill Point Types (DIN1412)











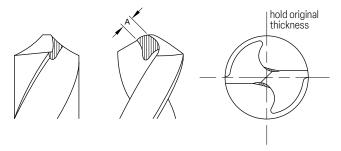
Drill Tolerances DIN / ISO 286, Part 2

| Drill Diameter at Point (mm) | | Diameter Tole | Back Taper (mm) | | | |
|------------------------------|-----------|---------------|-----------------|-------------------------|----|----------|
| Over | Inclusive | Plus (+) | Minus (-) | (Tapering of Diameter)† | | ameter)† |
| 0.20 | 3.00 | 0.000 | 0.014 | 0.000 | to | 0.008 |
| 3.00 | 6.00 | 0.000 | 0.018 | 0.002 | to | 0.008 |
| 6.00 | 10.00 | 0.000 | 0.022 | 0.002 | to | 0.009 |
| 10.00 | 18.00 | 0.000 | 0.027 | 0.003 | to | 0.011 |
| 18.00 | 30.00 | 0.000 | 0.033 | 0.004 | to | 0.015 |
| 30.00 | 50.00 | 0.000 | 0.039 | 0.004 | to | 0.015 |

 $^{^\}dagger$ The Drill diameter usually reduces towards the shank end; tolerance per 10mm of flute length.

Web Thinning

On most drills the web increases in thickness towards the shank with the result that, as the drill is shortened by repeated sharpening, the chisel edge will become wider. As the chisel edge does not cut but forces the metal out of the way, too wide a chisel edge will result in more pressure required for penetration, leading to greater heat generation and a resultant loss of life.



Cutting Fluids

The use of cutting fluids is an advantage in most drilling operations and an essential in some. The two main functions of the cutting fluid are lubrication and cooling. The purpose of lubrication is to reduce friction by lubricating the surfaces tool and work, to facilitate easier sliding of the chips up the flute and to prevent the chips welding to the cutting edges. In production work, particularly when drilling deep holes, the cooling action of the fluid is often more important than the lubrication. Overheating will shorten the life of the drill. Intermittent feed on deep holes, where possible, not only clears the chips but permits more effective cooling.

Speeds

The speed of a drill is the rate at which the periphery of the drill moves in relation to the work being drilled. As a rule, with a drill working within its speed range for a specific material, more holes between sharpening will be achieved if the speed is reduced and less holes if the speed is increased. Thus, for each production run, a speed must be established which will result in the highest rate of production without excessive breakdown time or drill usage. The factors governing speed are: component material, hardness of material, depth of hole, quality required, condition of drilling machine, efficiency of cutting fluid.

Feeds

The feed of the drill is governed by the drill size and the component material. As with speeds, an increase in feed will lessen the number of holes produced sharpening but it is essential that a constant feed be maintained. If a drill is allowed to dwell, breakdown of the cutting edges will result.

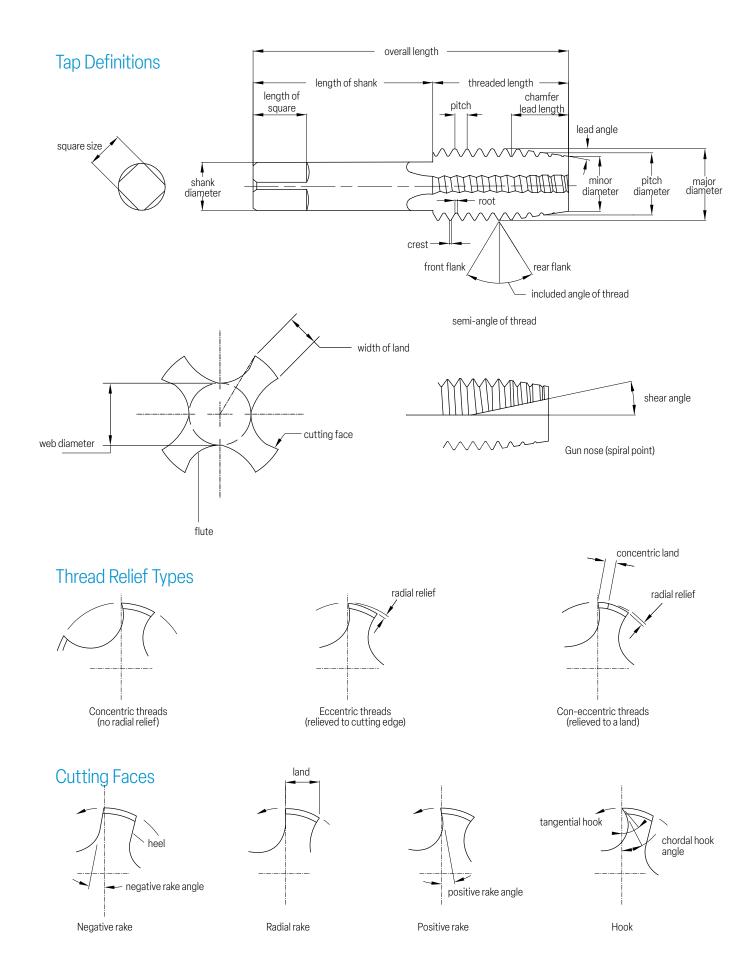
Small Drill Feeds and Speeds

Breakdown of small drills can most often be attributed to two faults: speed too high and feed too low. A feed which will produce CHIPS not POWDER, coupled with a speed compatible with the strength of the drill is essential for small hole drilling. Feeds must be based on thickness of chip, not mm/min, and speeds adjusted accordingly. EXAMPLE: A 1mm drill is to operate at a feed of 0.013mm /rev, drilling steel. While the material may permit a speed of 30m/min or 9,500 RPM it is obvious that the drill could not withstand a load of 0.013mm feed at this speed; a penetration rate of 124mm/min. The correct procedure is to retain the feed but reduce the speed to obtain a penetration within the capacity of the strength of the drill.

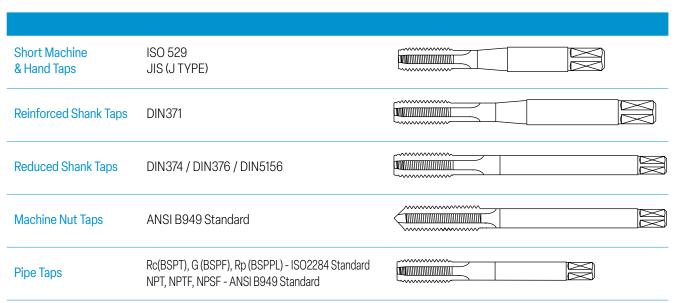
Deep Hole Drilling

When drilling deep holes, speeds and feeds should be reduced as follows:

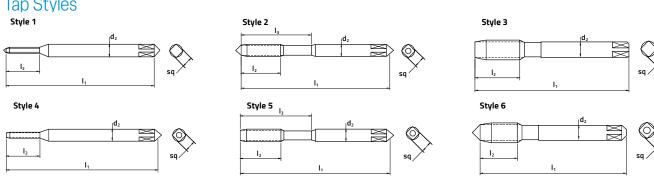
| Depth of hole | Reduction percent % | | |
|-----------------------------|---------------------|------|--|
| | Speed | Feed | |
| 3 times drill diameter | 10 | 10 | |
| 4 times drill diameter | 30 | 10 | |
| 5 times drill diameter | 30 | 20 | |
| 6 to 8 times drill diameter | 35 to 40 | 20 | |



Construction dimensions / designs



Tap Styles



Chamfer Type / Length

Table below is in accordance with ISO8830 / DIN2197

| Terminology | Form | Number of threads on lead | Chamfer angle (≈) | Type of flute | Main area of application | Illustration |
|--------------|------|---------------------------------|----------------------|-------------------------------|--|--------------|
| TAPER | A | 6 to 8 | 5° | Hand or straight flutes | Short through holes | |
| INTERMEDIATE | D | 3.5 to 5 | 8° | Hand or straight | Generally for through holes | |
| BOTTOMING | E* | 1.5 to 2 | 23° | Hand or straight flutes | Blind holes with very short thread run out | |
| INTERMEDIATE | В | 3.5 to 5 | 10° | Straight, with spiral point | Through holes in medium & long chipping materials | |
| BOTTOMING | С | 2 to 3 | 15° | Spiral fluted | Generally for blind holes | |

^{*} Use of this type is not recommended

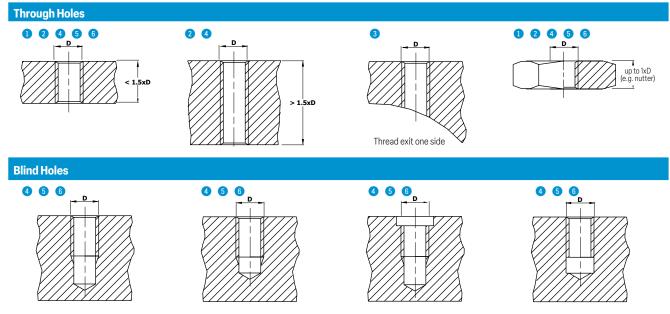
Tap Types - Helix direction/ Helical pitch / Fluteless

The helix angle depends primarily upon the hole form, eg. Through hole, blind hole, deep blind hole, etc., but the material, eg short chips, long chips, also has a strong influence on the direction of the helix. The following basic forms have derived during the development of taps:

Illustration ~~~~ 1 Straight Flutes (Hand) - Suitable for through or blind holes. The flutes only have room for a small amount of chips. The chips are not transported axially. Therefore, it is not advisable to cut deep through or blind holes (except in short chipping materials), with this type. Straight Flutes with (Gun) – Suitable for through holes, the gun point curls the chip forward ahead of the tap & out of the hole. Therefore, chip clogging is avoided and coolant can flow without problems. Spiral Flutes (LH Spiral, right hand cutting) - Suitable for interrupted through holes, where cross-holes exist. The direction of the flutes, curls & transports the chips forward of the tap, similar to Gun taps (also, opposite to RH spiral flutes). However, in applications where another hole intersects with the tapped hole, the helical flutes maintain the pitching of the thread. 4 15° Spiral Flutes (RH Spiral) – Suitable for blind holes, best suited to tough short chipping materials, up to 1.5 x D in depth. This particular tap design has no advantages for soft, and long chipping materials, especially over 1.5 x d, in depth. Due to the slow helix angle not transporting the chips well, clogging is possible. 5 40° to 50° Spiral Flutes (RH Spiral) – Suitable for blind holes, best suited to long chipping materials, the high helix angle & the direction of the flutes, curls & transports the chips back out of the hole. This particular tap style is required to cut on reversal; therefore flute rake is required on the both front & back flute faces. Thredflo/Roll taps (fluteless) - Suitable for blind & through holes. This type of tap internally rolls a thread, therefore displacing the metal rather than cutting, like the above mentioned styles. Due to torque generated when producing roll threads, much higher machine power is required. Roll threads also produce much stronger threads than cut threads, as the grain structure of the thread remains uniform through the thread form profile. Note! Tapping drill size is not the same as a cut thread tap.

The above basic tool types are available in different variations, which have been designed & developed in respect to the specific materials and working conditions.

Tap Hole Types



For blind holes, there are generally two thread run out forms used at the bottom of the tap hole. One form has a recessed diameter at the bottom of the hole, and the other form has a standard run out. Other types of holes are respective to construction designs, eg.

- a) The bore is smaller than the tap hole diameter (typical for pipes)
- b) As step hole, where the following diameter (second step), is smaller than the tap hole diameter.

Technical Information Tap Geometry

sutton

Geometry

| Sutton Designation | Description | Tap geometry | Surface |
|-----------------------|---|--|---------------------------|
| GG | For cast iron – iron is a very abrasive material, therefore to increase tool life the taps are always surface treated or coated to resist the abrasion. The thread limit for this range is 6HX, which is high limit of the 6H tolerance allowing for longer wear life. | Straight flutes with low rake angle | TiCN Plasma Nitride Ni |
| N | For normal, general purpose type materials – suited to a wide range of materials, with normal rakes & relief's. This is existing geometry that Sutton Tools has historically manufactured. | Normal rake angle & normal thread relief | Bright Blu TiN |
| UNI | For normal, general purpose type materials – suited to a wide range of materials, with normal rakes & high relief's. However tap material is powder metal high speed steel (PM-HSS), which due to its finer grain structure than that of conventional HSS, higher hardness can be achieved with excellent toughness, along with TiAIN surface coating allowing for better tool life than normal taps. | Normal rake angle & high thread relief | Bright TiAIN |
| VA | For stainless and tough steels – to avoid clogging in tough, long chipping materials such as stainless steel, it is essential that the chip flows continuously in an axial direction. Best suited to rigid tapping applications due to high thread relief. TiCN & TiN coating has proven to be best suited for these materials. | High rake angle & thread relief | TiCN Blu |
| VAPM | For stainless and tough steels – geometry similar to VA range, however tap material is powder metal high speed steel (PM-HSS), which due to its finer grain structure than that of conventional HSS, higher hardness can be achieved with excellent toughness, allowing for better tool life than VA taps. | High rake angle & thread relief | TiCN |
| Н | For hard materials forming short chips – the low rakes & relief's combined with a hard surface coating, allow excellent tool life. | Low rake angle & thread relief | TiCN |
| w | For soft materials – due to the very high rake angle with a low thread relief, allows for excellent chip flow & gauging in soft materials. | High rake angle & low thread relief | Bright CrN |
| Al | For malleable aluminium with long chips – to avoid clogging when threading in aluminium which forms long chips, it is essential that the chip flows continuously in an axial direction. Generally these taps have 1 less flute than normal taps & therefore have larger flute space, which more adequate for large volumes of chips to help avoid clogging. | High rake angle, high helix, 2 flutes, low thread relief | Bright Plasma Nitride |



Lubricants

Hee.

Use of a suitable lubricant or cutting compound is necessary on most tapping operations. The type of lubricant as well as the method of application is often of extreme importance and can be responsible for the success or failure of a tapping operation.

Recommendation:

Better results can sometimes be obtained by the use of one of the many modified or specialised lubricants recommended by cutting oil specialists.

The general principle is to have more EP (Extreme Pressure) additives added with the degree of difficulty, usually hardness increase. Oils stick, and improve frictional properties essential in tapping tough applications.

Application:

Proper application of the lubricant is just as important as the type used. To be effective, ample quantities of lubricant must reach the chamfer or cutting portion of the tap during the entire tapping operation. In many cases, the lubricant must also aid in controlling or disposing of the chips.

Flow:

The flow of lubricant should be directed into the hole rather than at the tap and should have sufficient pressure to wash the chips away from the hole as much as possible. Also, if the flow is not continuous, it should start before the tap enters the hole and continuou until the tap is completely reversed out of the hole. In this way, ample oil is provided at the start of the cut and loose chips will be suspended in the oil so that they do not interfere with the tap backing out of the hole. On machines where the work revolves and the tap is stationary, it is desirable to use several streams of lubricant on opposite sides of the tap, especially on horizontal tapping.

Cleanliness:

Tapping lubricants must always be clean. If filter equipment is not used, the lubricant must be replaced periodically to eliminate fine chips, grit and foreign matter that accumulate in the tank. Also, it is very important that the piping and tank are thoroughly flushed and cleaned before filling with new lubricant. The dilution of lubricants often changes during use so that additions may be necessary to maintain the recommended proportion of active materials.

Tapping drill

The tapping drill hole diameter should be drilled as large as possible, within the respective fitting just under the upper permissible dimension of the tolerance. If the tapping drill hole diameter is too small, then this will cause the thread root diameter (minor diameter) to cut the material. This should be avoided, because the small chips which derive from the root of thread, clog the normal chip flow and rip pieces of material out of the finished thread. Consequently, the tap is overloaded and often breaks because of the high torque.

Another problem which occurs in certain materials due to thread root diameter cutting, is when a chip-bulge has been formed around the root radius. The minor diameter of the tap is clogged with small chips, which leads to a clamping of the tool teeth are ripped out, which leads to tool breakage. It is therefore, necessary that the material which is to be tapped, be taken into account when determining the tap hole diameter. Typical materials which do not squeeze or clamp are iron, brass and bronze and materials which squeeze are steels, steel castings and malleable steels. The tap cuts more economically, when the tap drill hole diameter is within the upper range of the permissible tolerance.

Warning: When drilling holes in materials which tend to work harden, care is needed to ensure the drills are sharp otherwise tap life is decreased.

Tapping drill formula

The correct size of drill to give the desired percentage of thread can be calculated by using the following formula:

| Thread Type | Formula | Example |
|--|--|--|
| Metric (ISO) | Drill Size = Nom, Tap Dia, in mm – Pitch | M6 × 1 = 5.00mm drill |
| Whitworth Form Threads (inch calculation) | Drill Size = Nom, Tap Dia, - 1.28 TPI of thread depth | 1/4 BSW 75% thread required: Drill Size = 0.250 - \(\frac{1.28}{20}\) - \(\frac{75}{10}\) 250 - 0.048 Therefore Drill Size = 0.202 Nearest Standard Drill = 5.1mm = 0.2007 inch |
| Unified Form Threads (inch calculation) | Drill Size = Nom, Tap Dia, - 1.30 TPI | 1/4 UNC 75% thread required: Drill Size = 0.250 - \(\frac{1.30}{20} \) - \(\frac{75}{100} \) .250 - 0.049 Therefore Drill Size = 0.201 Nearest Standard Drill = 5.1mm = 0.2007 inch |

All sizes are "suggested sizes" only and may be varied to suit individual requirements

| M (200) | | | | |
|-------------|-------------------------|---------------------|--|--|
| ISON | ISO Metric Coarse (60°) | | | |
| Tap Size | Pitch mm | Tapping Drill mm | | |
| M1.6 | 0.35 | 1.25 | | |
| M2 | 0.4 | 1.6 | | |
| M2.5 | 0.45 | 2.05 | | |
| M3 | 0.5 | 2.5 | | |
| M3.5 | 0.6 | 2.9 | | |
| M4 | 0.7 | 3.3 | | |
| M4.5 | 0.75 | 3.7 | | |
| M5 | 0.8 | 4.2 | | |
| M6 | 1.0 | 5.0 | | |
| M8 | 1.25 | 6.8 | | |
| M10 | 1.5 | 8.5 | | |
| M12 | 1.75 | 10.2 | | |
| M14 | 2.0 | 12.0 | | |
| M16 | 2.0 | 14.0 | | |
| M18 | 2.5 | 15.5 | | |
| M20 | 2.5 | 17.5 | | |
| M22 | 2.5 | 19.5 | | |
| M24 | 3.0 | 21.0 | | |
| M27 | 3.0 | 24.0 | | |
| M30 | 3.5 | 26.5 | | |
| M33 | 3.5 | 29.5 | | |
| M36 | 4.0 | 32.0 | | |
| M42 | 4.5 | 37.5 | | |
| M45 | 4.5 | 40.5 | | |
| M48 | 5.0 | 43.0 | | |
| M52 | 5.0 | 47.0 | | |
| M56 | 5.5 | 50.5 | | |

ISO Metric Fi

Size

M4

M6 M8

M10

M12**

M12

M14** M14

M16*

M18**

M20* M22

M24

M25*

M32* M40*

M50*

M5

Pitch

mm

0.5

0.75

1.0

1.25

1.25

1.5

1.5

1.5

1.5

1.5

2.0

1.5

1.5

1.5

| | 17.5 | |
|-------|--|---|
| | 19.5 | |
| | 21.0 | |
| | 24.0 | |
| | 26.5 | |
| | 29.5 | |
| | 32.0 | |
| | 37.5 | |
| | 40.5 | |
| | 43.0 | |
| | 47.0 | |
| | 50.5 | - |
| | | |
| | 0.00) | _ |
| ne ((| 60°) | |
| , , | | |
| | | |
| | Tapping Drill mm | |
| | Tapping Drill mm | - |
| | Tapping Drill mm 3.5 | - |
| | Tapping Drill mm 3.5 4.5 | - |
| | Tapping Drill mm 3.5 4.5 5.3 | - |
| | Tapping Drill mm 3.5 4.5 | - |
| | Tapping Drill mm 3.5 4.5 5.3 7.0 | - |
| | Tapping Drill mm 3.5 4.5 5.3 7.0 9.0 8.8 | - |
| | Tapping Drill mm 3.5 4.5 5.3 7.0 9.0 | |
| | Tapping Drill mm 3.5 4.5 5.3 7.0 9.0 8.8 10.8 10.5 12.8 | |
| | Tapping Drill mm 3.5 4.5 5.3 7.0 9.0 8.8 10.8 10.5 | |
| | Tapping Drill mm 3.5 4.5 5.3 7.0 9.0 8.8 10.8 10.5 12.8 | |
| | Tapping Drill mm 3.5 4.5 5.3 7.0 9.0 8.8 10.8 10.5 12.8 12.5 | |
| | Tapping Drill mm 3.5 4.5 5.3 7.0 9.0 8.8 10.8 10.5 12.8 12.5 14.5 16.5 18.5 | |
| | Tapping Drill mm 3.5 4.5 5.3 7.0 9.0 8.8 10.8 10.5 12.8 12.5 14.5 16.5 | |
| | Tapping Drill mm 3.5 4.5 5.3 7.0 9.0 8.8 10.8 10.5 12.8 12.5 14.5 16.5 18.5 | |

38.5 48.5

*UNS

*Metric Conduit **Spark Plug

| 8UN (8 TPI) Unified National Form (60°) | | | |
|---|--------|---------------------|--|
| Tap Size | T.P.I. | Tapping Drill mm | |
| 1-1/8 | 8 | 25.5 | |
| 1-1/4 | 8 | 28.5 | |
| 1-3/8 | 8 | 31.75 | |
| 1-1/2 | 8 | 35.0 | |
| 1-5/8 | 8 | 38.0 | |
| 1-3/4 | 8 | 41.5 | |
| 1-7/8 | 8 | 44.5 | |
| 2 | 8 | 47.5 | |

| UNC Unified National Coarse (60°) | | | | |
|---|--------------|----------------------|--|--|
| Tap Size | T.P.I. | Tapping Drill mm | | |
| #2 (0.086) | 56 | 1.85 | | |
| #3 (0.099) | 48 | 2.1 | | |
| #4 (0.112) | 40 | 2.3 | | |
| #5 (0.125) | 40 | 2.6 | | |
| #6 (0.138) | 32 | 2.8 | | |
| #8 (0.164) | 32 | 3.4 | | |
| #10 (0.190) | 24 | 3.8 | | |
| #12 (0.216) | 24 | 4.5 | | |
| 1/4 | 20 | 5.1 | | |
| 5/16 | 18 | 6.6 | | |
| 3/8 | 16 | 8.0 | | |
| 7/16 | 14 | 9.4 | | |
| 1/2 | 13 | 10.8 | | |
| 9/16 | 12 | 12.2 | | |
| 5/8 | 11 | 13.5 | | |
| 3/4 7/8 | 10 9 8 | 16.5 19.5 22.2 | | |
| 1-1/8 | 7 | 25.0 | | |
| 1-1/4 | 7 | 28.0 | | |
| 1-3/8 | 6 | 31.0 | | |
| 1-1/2 | 6 | 34.0 | | |
| 1-3/4 | 5 | 39.5 | | |
| 2 | 4.5 | 45.0 | | |

UNF

| Unified National Fine (60°) | | | | |
|-----------------------------|--------|---------------------|--|--|
| Tap Size | T.P.I. | Tapping Drill mm | | |
| #3 (0.099) | 56 | 2.1 | | |
| #4 (0.112) | 48 | 2.35 | | |
| #5 (0.125) | 44 | 2.65 | | |
| #6 (0.138) | 40 | 2.9 | | |
| #8 (0.164) | 36 | 3.5 | | |
| #10 (0.190) | 32 | 4.1 | | |
| #12 (0.216) | 28 | 4.6 | | |
| 3/16* | 32 | 4.0 | | |
| 1/4 | 28 | 5.5 | | |
| 5/16 | 24 | 6.9 | | |
| 3/8 | 24 | 8.5 | | |
| 7/16 | 20 | 9.8 | | |
| 1/2 | 20 | 11.5 | | |
| 9/16 | 18 | 12.8 | | |
| 5/8 | 18 | 14.5 | | |
| 3/4 | 16 | 17.5 | | |
| 7/8 | 14 | 20.5 | | |
| 1 | 12 | 23.5 | | |
| 1* | 14 | 24.0 | | |
| 1-1/8 | 12 | 26.5 | | |
| 1-1/4 | 12 | 29.5 | | |
| 1-3/8 | 12 | 33.01 | | |
| 1-1/2 | 12 | 36.0 | | |

| UNEF Unified National Form (60°) | | | | |
|---|--------|---------------------|--|--|
| Tap Size | T.P.I. | Tapping Drill mm | | |
| 1/4 | 32 | 5.6 | | |
| 5/16 | 32 | 7.2 | | |
| 3/8 | 32 | 8.8 | | |
| 1/2 | 28 | 11.8 | | |
| 5/8 | 24 | 14.75 | | |
| 3/4 | 20 | 18 | | |
| 1 | 20 | 24 2 | | |

| BSW | | | | |
|----------------------------------|--------|---------------------|--|--|
| British Standard Whitworth (55°) | | | | |
| Tap Size | T.P.I. | Tapping Drill mm | | |
| 1/16* | 60 | 1.2 | | |
| 3/32* | 48 | 1.85 | | |
| 1/8 | 40 | 2.55 | | |
| 5/32* | 32 | 3.2 | | |
| 3/16 | 24 | 3.7 | | |
| 7/32* | 24 | 4.5 | | |
| 1/4 | 20 | 5.1 | | |
| 5/16 | 18 | 6.5 | | |
| 3/8 | 16 | 7.9 | | |
| 7/16 | 14 | 9.3 | | |
| 1/2 | 12 | 10.5 | | |
| 9/16 | 12 | 12.1 | | |
| 5/8 | 11 | 13.5 | | |
| 3/4 | 10 | 16.25 | | |
| 7/8 | 9 | 19.25 | | |
| 1 | 8 | 22.0 | | |
| 1-1/8 | 7 | 24.75 | | |
| 1-1/4 | 7 | 28.0 | | |
| 1-1/2 | 6 | 33.5 | | |
| 1-3/4 | 5 | 39.0 | | |
| 2 | 4-1/2 | 44.5 | | |

*WHIT. Form

| BSF British Standard Fine (55°) | | | |
|---|--------|---------------------|--|
| Tap Size | T.P.I. | Tapping Drill mm | |
| 3/16 | 32 | 4.0 | |
| 7/32 | 28 | 4.6 | |
| 1/4 | 26 | 5.3 | |
| 5/16 | 22 | 6.8 | |
| 3/8 | 20 | 8.3 | |
| 7/16 | 18 | 9.8 | |
| 1/2 | 16 | 11.0 | |
| 9/16 | 16 | 12.7 | |
| 5/8 | 14 | 14.0 | |
| 11/16 | 14 | 15.5 | |
| 3/4 | 12 | 16.75 | |
| 7/8 | 11 | 19.75 | |
| 1 | 10 | 22.75 | |
| 1-1/8 | 9 | 25.5 | |
| 1-1/4 | 9 | 28.5 | |
| 1-1/2 | 8 | 34.5 | |
| 1-3/4 | 7 | 41.0 | |

| BSB British Standard Brass (55°) | | | | |
|--|--------|---------------------|--|--|
| Tap Size | T.P.I. | Tapping Drill mm | | |
| 1/4 | 26 | 5.2 | | |
| 5/16 | 26 | 6.8 | | |
| 3/8 | 26 | 8.4 | | |
| 7/16 | 26 | 10.0 | | |
| 1/2 | 26 | 11.6 | | |
| 9/16 | 26 | 13.2 | | |
| 5/8 | 26 | 14.8 | | |
| 3/4 | 26 | 18.0 | | |
| 7/8 | 26 | 20.8 | | |
| 1 | 26 | 24.3 | | |

| Rc (BSPT)* ISO Rc Taper Series 1:16 (55°) | | | | |
|---|--------|----------------|-------------------|--|
| Tap Size | T.P.I. | Drill Only* | Drill & Reamer | |
| Rc 1/16 | 28 | 6.4 | 6.2 | |
| Rc 1/8 | 28 | 8.4 | 8.4 | |
| Rc 1/4 | 19 | 11.2 | 10.8 | |
| Rc 3/8 | 19 | 14.75 | 14.5 | |
| Rc 1/2 | 14 | 18.25 | 18.0 | |
| Rc 3/4 | 14 | 23.75 | 23.0 | |
| Rc 1 | 11 | 30.0 | 29.0 | |
| Rc 1-1/4 | 11 | 38.5 | 38.0 | |
| Rc 1-1/2 | 11 | 44.5 | 44.0 | |
| Rc 2 | 11 | 56.0 | 55.0 | |

| G (BSPF) ISO G Parallel Series (55°) | | | | |
|--|--------|---------------------|--|--|
| Tap Size | T.P.I. | Tapping Drill mm | | |
| G1/16 | 28 | 6.8 | | |
| G1/8 | 28 | 8.8 | | |
| G1/4 | 19 | 11.8 | | |
| G 3/8 | 19 | 15.3 | | |
| G1/2 | 14 | 19.0 | | |
| G 5/8 | 14 | 21.0 | | |
| G 3/4 | 14 | 24.5 | | |
| G7/8 | 14 | 28.5 | | |
| G1 | 11 | 31.0 | | |
| G1-1/4 | 11 | 39.5 | | |
| G1-1/2 | 11 | 45.5 | | |
| G1-3/4 | 11 | 51.5 | | |
| G 2 | 11 | 57.5 | | |
| G 2-1/2 | 11 | 72.5 | | |

| Rp (BSPPL) Sealing pipe thread parallel (55°) | | | | | |
|---|----|------|--|--|--|
| Tap T.P.I. Tapping Dri | | | | | |
| Rp 1/8 | 28 | 8.6 | | | |
| Rp 1/4 | 19 | 11.5 | | | |
| Rp 3/8 | 19 | 15.0 | | | |
| Rp 1/2 | 14 | 18.5 | | | |
| Rp 3/4 | 14 | 24.0 | | | |
| Rp 1 | 11 | 30.2 | | | |
| Rp 1-1/4 | 11 | 39.0 | | | |
| Rp 1-1/2 | 11 | 45.0 | | | |
| Rp 2 | 11 | 56.4 | | | |

| Pg Steel conduit (80°) | | | | |
|----------------------------------|--------|---------------------|--|--|
| Tap Size | T.P.I. | Tapping Drill mm | | |
| Pg7 | 20 | 11.3 | | |
| Pg9 | 18 | 13.9 | | |
| Pg11 | 18 | 17.3 | | |
| Pg13.5 | 18 | 19.1 | | |
| Pg16 | 18 | 21.2 | | |
| Pg21 | 15 | 26.8 | | |
| | | | | |

| Thread forming (Fluteless taps) | | | | |
|---|--------------|---------------------|--|--|
| Tap Size | T.P.I. | Tapping Drill mm | | |
| | Metric coars | e | | |
| M1 | 0.25 | 0.9 | | |
| M1.1 | 0.25 | 1.0 | | |
| M1.2 | 0.25 | 1.1 | | |
| M1.4 | 0.3 | 1.28 | | |
| M1.6 | 0.35 | 1.45 | | |
| M1.7 | 0.35 | 1.55 | | |
| M1.8 | 0.35 | 1.65 | | |
| M2.0 | 0.40 | 1.8 | | |
| M2.2 | 0.45 | 2.0 | | |
| M2.3 | 0.4 | 2.1 | | |
| M2.5 | 0.45 | 2.3 | | |
| M2.6 | 0.45 | 2.4 | | |
| M3 | 0.5 | 2.8 | | |
| M3.5 | 0.6 | 3.2 | | |
| M4 | 0.7 | 3.7 | | |
| M5 | 0.8 | 4.6 | | |
| M6 | 1.0 | 5.5 | | |
| M8 | 1.25 | 7.4 | | |
| M10 | 1.5 | 9.3 | | |
| M12 | 1.75 | 11.2 | | |
| | BSW | | | |
| 1/8 | 40 | 2.9 | | |
| 5/32 | 32 | 3.6 | | |
| 3/16 | 24 | 4.3 | | |
| 1/4 | 20 | 5.8 | | |
| 5/16 | 18 | 7.3 | | |
| 3/8 | 16 | 8.8 | | |
| | | | | |

| NPT-NPTF* National Pipe Taper 1:16 (60°) | | | | |
|--|--------|-------------------|------|--|
| Tap Size | T.P.I. | Drill & Reamer | | |
| 1/16 | 27 | 6.3 | 6.0 | |
| 1/8 | 27 | 8.5 | 8.2 | |
| 1/4 | 18 | 11.0 | 10.8 | |
| 3/8 | 18 | 14.5 | 14.0 | |
| 1/2 | 14 | 18.0 | 17.5 | |
| 3/4 | 14 | 23.0 | 23.0 | |
| 1 | 11-1/2 | 29.0 | 28.5 | |
| 1-1/4 | 11-1/2 | 37.5 | 37.0 | |
| 1-1/2 | 11-1/2 | 44 | 43.5 | |
| 2 | 11-1/2 | 55.5 | 55.0 | |

| NPSF National Pipe Straight (60°) | | | | |
|---|---------------------|------|--|--|
| Tap Size | Tapping Drill mm | | | |
| 1/8 | 27 | 8.6 | | |
| 1/4 | 18 | 11.3 | | |
| 3/8 | 18 | 14.5 | | |
| 1/2 | 14 | 18.0 | | |

^{*}Taper pipe threads of improved quality are obtained when taper is pre-formed using Sutton Tools Taper Pipe Reamers.

| Thread forming (Fluteless taps) | | | |
|------------------------------------|----------|---------------------|--|
| Tap Size | T.P.I. | Tapping Drill mm | |
| | UNC | | |
| #1 (0.073) | 64 | 1.7 | |
| #2 (0.086) | 56 | 2.0 | |
| #3 (0.099) | 48 | 2.3 | |
| #4 (0.112) | 40 | 2.6 | |
| #5 (0.125) | 40 | 2.9 | |
| #6 (0.138) | 32 | 3.2 | |
| #8 (0.164) | 32 | 3.8 | |
| #10 (0.190) | 24 | 4.4 | |
| #12 (0.216) | 24 | 5.0 | |
| 1/4 | 20 | 5.8 | |
| 5/16 | 18 | 7.3 | |
| 3/8 | 16 | 8.8 | |
| 7/16 | 14 | 10.2 | |
| 1/2 | 13 | 11.7 | |
| | UNF | | |
| #1 (0.073) | 72 | 1.7 | |
| #2 (0.086) | 64 | 2.0 | |
| #3 (0.099) | 56 | 2.3 | |
| #4 (0.112) | 48 | 2.6 | |
| #5 (0.125) | 44 | 2.9 | |
| #6 (0.138) | 40 | 3.2 | |
| #8 (0.164) | 36 | 3.9 | |
| #10 (0.190) | 32 | 4.5 | |
| #12 (0.216) | 28 | 5.1 | |
| 1/4 | 28 | 6.0 | |
| 5/16 | 24 | 7.5 | |
| 3/8 | 24 | 9.0 | |
| 7/16 | 20 | 10.6 | |
| 1/2 | 20 | 12.1 | |
| | G (BSPF) | | |
| 1/8 | 28 | 9.25 | |
| 1/4 | 19 | 12.5 | |
| 3/8 | 19 | 16.0 | |
| 1/2 | 14 | 20.0 | |
| 5/8 | 14 | 22.0 | |
| 3/4 | 14 | 25.5 | |
| 7/8 | 14 | 29.25 | |
| 1 | 11 | 32.0 | |

| | BA (47.5°) | |
|-------------|----------------------|---------------------|
| Tap Size | Pitch mm | Tapping Drill mm |
| 0 | 1 | 5.1 |
| 1 | 0.9 | 4.5 |
| 2 | 0.81 | 4.0 |
| 3 | 0.73 | 3.4 |
| 4 | 0.66 | 3.0 |
| 5 | 0.59 | 2.65 |
| 6 | 0.53 | 2.3 |
| 7 | 0.48 | 2.05 |
| 8 | 0.43 | 1.8 |
| 9 | 0.39 | 1.55 |
| 10 | 0.35 | 1.4 |
| 11 | 0.31 | 1.2 |
| 12 | 0.28 | 1.05 |
| 13 | 0.25 | 0.98 |
| 14 | 0.23 | 0.8 |
| 15 | 0.21 | 0.7 |
| 16 | 0.19 | 0.6 |

Fluteless taps

Fluteless taps do not cut threads in the same manner as conventional taps – but actually FORM and FLOW the threads with an absence of chips. Used under suitable conditions, these taps produce threads with a high degree of finish not possible with ordinary taps. Ductile materials are most appropriate for forming of threads and must have a minimum 10% elongation.

Benefits of thread forming

- · Higher speeds and tool life
- · Reduced possibility of breakage due to no cutting edges and robust tool construction

Figure 1. No chips produced

Figure 2. Higher tensile strength threads produced due to grain structure following the thread form

Figure 3. For use in through and blind holes applications

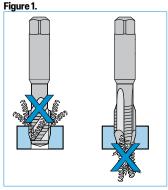
What's New?

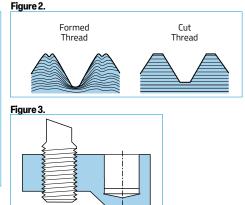
Figure 4. New polygon profile

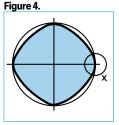
Figure 5. New radiused blend on polygon profile

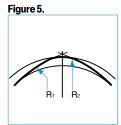
Figure 6. Thread profile with radius crest

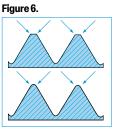
Figure 7. Polished tool surface, surface finish













Suitable for wide range materials

- -Low carbon steels
- -Leaded steels
- -Austenitic stainless steels
- -Alloy steels; typically up to 1200 N/mm², (36 Rc) with a minimum 10% elongation
- -Aluminium die castings alloys (low silicon, 10% max;)
- -Wrought aluminium alloys (Ductile)
- -Zinc die casting alloys
- -Copper and copper alloys

Percentage of thread required

Because the thread produced by a fluteless tap is substantially stronger than a conventional thread, greater tool life and efficiency may be obtained when forming up to 65% thread

Threads may be formed up to 80% of depth, but tool life will be reduced and work clamping pressure necessarily increased. Greater tapping speeds allow the metal to flow far more readily, so 60 feet per minute minimum may be used as a guide, but this could increase with the type of material being tapped. A depth of 65% is recommended for the ductile materials mentioned, but this percentage will be reduced for less ductile materials to maintain all-round efficiency.

Tapping drill formula for fluteless taps

Refer Tapping Drill Size Chart for recommended sizes (Suitable for Unified, Whitworth and Metric sizes only). The formula to calculate the theoretical hole size for a required percentage of thread is:

| Formula Example | | |
|---|--|--|
| Drill size = nominal thread dia. (in mm)- (0.007 x % of thread x pitch) | Drill size for 65% of thread in a M6 x 1.0 threaded hole would be: Drill size = $6 - (0.007 \times 65 \times 1.0 \text{ (pitch)}) = 5.54 \text{mm}$ | |
| Drill size = nominal thread dia. (in mm)- (0.007 x % or thread x pitch) | (Use 5.50mm drill (Stockable drill) = 71%) | |

It is to be noted that the drill size for fluteless tapping is always larger than the P.D. of the thread. A drill size equal to the P.D. of the thread would produce 100% of thread, but this is NOT recommended.

As the additional driving torque is only up to 50% increase, any conventional driving equipment using the square as a drive is suitable for fluteless tapping.

Lubrication

In general it is best to use a good cutting oil or lubricant rather than a coolant for fluteless tapping. Sulphur base and mineral oils, along with most friction reducing lubricants recommended for use in cold extrusion or metal drawing, have proven best for this work. Make sure lubricant is clean, free from chips swarf and fillings in suspension, which produce a poor finish and jamming, sometimes breakage – extra filtration may be required.

Countersinking

Because the fluteless tap displaces metal, some metal will be displaced above the mouth of the hole during tapping, countersink or chamfer the hole prior to tapping will reduce the extrusion within the countersink and not interfere with the mating part.

(Fluteless) Roll Taps:

| | Thread Size | | ISO Coarse | | UNC BSW | | D Coarse UNC BSW | | SW |
|--------|-------------|--------------------|-------------|---------------------|---------|---------------------|------------------|---------------------|----|
| Metric | Fraction | M/C Screw Gauge | Pitch mm | Tapping Drill mm | T.P.I. | Tapping Drill mm | T.P.I. | Tapping Drill mm | |
| M1.0 | | | 0.25 | 0.90 | | | | | |
| M1.1 | | | 0.25 | 1.00 | | | | | |
| M1.2 | | | 0.25 | 1.10 | | | | | |
| M1.4 | | | 0.3 | 1.25 | | | | | |
| M1.6 | | | 0.35 | 1.45 | | | | | |
| M1.7 | | | 0.35 | 1.55 | | | | | |
| M1.8 | | | 0.35 | 1.65 | | | | | |
| M2.0 | | | 0.4 | 1.80 | | | | | |
| M2.2 | | | 0.45 | 2.00 | | | | | |
| M2.3 | | | 0.4 | 2.10 | | | | | |
| M2.5 | | | 0.45 | 2.30 | | | | | |
| M2.6 | | | 0.45 | 2.40 | | | | | |
| M3.0 | | | 0.5 | 2.75 | | | | | |
| | 1/8 | | | | | | 40 | 2.90 | |
| M3.5 | | | 0.6 | 3.20 | | | | | |
| | | #6 | | | 32 | 3.10 | | | |
| | 5/32 | | | | | | 32 | 3.60 | |
| M4 | | | 0.7 | 3.70 | | | | | |
| | | #8 | | | 32 | 3.80 | | | |
| | 3/16 | | | | | | 24 | 4.30 | |
| | | #10 | | | 24 | 4.30 | | | |
| M5 | | | 0.8 | 4.60 | | | | | |
| M6 | | | 1.0 | 5.55 | | | | | |
| | 1/4 | | | | 20 | 5.80 | 20 | 5.80 | |
| | 5/16 | | | | 18 | 7.30 | 18 | 7.30 | |
| M8 | | | 1.25 | 7.40 | | | | | |
| | 3/8 | | | | 16 | 8.80 | 16 | 8.80 | |
| M10 | | | 1.50 | 9.30 | | | | | |
| | | | | | | | | | |

Thread Systems

The ISO standard is the international standard intended to be adopted throughout the world to unify and rationalise screw threads at an international level. The ISO standard recognises two groups of screw threads, (a) ISO metric, a complete thread system in metric units and (b) ISO inch Unified which is covered by British Standard BS 1580 and American Standard ANSI – B1-1 – Unified screw thread systems. The Whitworth and BA screw threads are obsolete but still widely used during the period of transition.

All measurements must have a controlling point or base from which to start. In the case of a screw thread, this control point is called BASIC or theoretically correct size, which is calculated on the basis of a full thread form. Thus, on a given screw thread, we have the Basic Major Diameter, the Basic Pitch Diameter, and the Basic Minor Diameter. The Basic Profile is the profile to which the deviations, which define the limits of the external and internal threads, are applied.

While it is impossible in practice to form screw threads to their precise theoretical or BASIC sizes, it is possible and practical to establish limits to which the deviation must not exceed. These are called the "Maximum" and "Minimum" Limits. If the product is no smaller than the "Minimum Limit" and no larger than the "Maximum Limit", then it is within the size limits required. This difference between the Maximum and Minimum Limits is the TOLERANCE. In actual practice, the Basic size is not necessarily between Maximum and Minimum Limits. In most cases, the Basic Size is one of the Limits.

In general, tolerances for internal threads will be above Basic and for external threads, below Basic.

Basic Profile for ISO Inch (Unified) and ISO Metric

The basic form is derived from an equilateral triangle which is truncated 1/8 of the height at the major diameter and 1/4 of the height at the minor diameter.

The corresponding flats have a width of P/8 and P/4 respectively. Figure 1.

In practice major diameter clearance is provided by the tap beyond the P/8 flat on internal threads and beyond the P/4 flat on external threads.

These clearances are usually rounded.

ISO Metric Tolerance Positions

Three tolerance positions are standardised for bolts and two for nuts. These are designated e, g and h for bolts and G and H for nuts. As in the ISO System for limits and fits, small letters are used to designate tolerance positions for bolts and capital letters are used for nut tolerance positions. Also the letters h and H are used for tolerance positions having the maximum metal limit coincided with the basic size, i.e., with a fundamental deviation of zero. **Figure 2**.

ISO Metric Tolerance Grades

A series of tolerance grades designated 4, 5, 6, 7 and 8 for nut pitch diameters.

An extended series of tolerance grades, designated 3, 4, 5, 6, 7,8 and 9, for bolt pitch diameters.

An important factor here is that for the same tolerance grade the nut pitch diameter tolerance is 1.32 x the corresponding bolt pitch diameter tolerance. Size and recommendations of fits can be obtained from the Australian Standards AS 1275 or AS 1721.

Figure 1

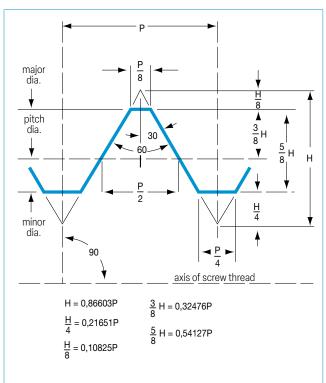
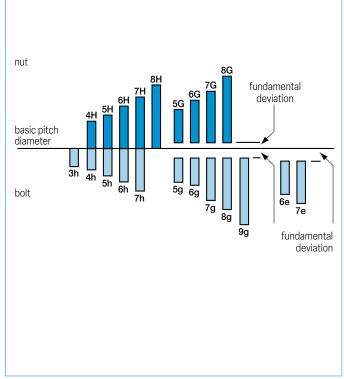


Figure 2



Technical Information Thread Limits

sutton

Metric Taps; Comparison Tap Limits & Product Classes and Grades

| Product Tolerance | | | | | | Tap Limits | | | | |
|-------------------|--------|------------------|-----------------------|--------------------------|-----------|------------|--------|----------|------------|----------|
| | | ISO Tolerance | 6H Upper Deviation | JIS 2 Old/JIS Product | Is | so | | Recomme | nded Limit | |
| Tap Size | Pitch | Class | Tolerance | Tolerance | Tap Grade | Tap Limits | P1 | P2 | Р3 | P4 |
| mm | 0.05 | 511 | μm | μm | | Microns µm | μm | μm | μm | μm |
| M1.0 | x 0.25 | 5H | 56 | 60 | ISO 1 | + 6 / 17 | +10/25 | | | |
| M1.1 | x 0.25 | 5H | 56 | 60 | ISO 1 | + 6 / 17 | +10/25 | | | |
| M1.2 | x 0.25 | 5H | 56 | 60 | ISO 1 | + 6 / 17 | +10/25 | | | |
| M1.4 | x 0.3 | 5H | 60 | 60 | ISO 1 | + 6 / 18 | +10/25 | | | |
| M1.6 | x 0.35 | 5H | 67 | 85 | ISO 1 | + 7/20 | +10/25 | + 25 /40 | | |
| M1.7 | x 0.35 | 6H | 85 | 85 | ISO 2 | +20/34 | +10/25 | + 25 /40 | | |
| M1.8 | x 0.35 | 6H | 85 | 85 | ISO 2 | +20/34 | +10/25 | + 25 /40 | | |
| M2.0 | x 0.4 | 6H | 90 | 70 | ISO 2 | +21/36 | +10/25 | + 25 /40 | | |
| M2.2 | x 0.45 | 6H | 95 | 95 | ISO 2 | +23/38 | +10/25 | + 25 /40 | | |
| M2.3 | x 0.4 | 6H | 90 | 95 | ISO 2 | +21/36 | +10/25 | + 25 /40 | | |
| M2.5 | x 0.45 | 6H | 95 | 95 | ISO 2 | +23/38 | +10/25 | + 25 /40 | | |
| M2.6 | x 0.45 | 6H | 95 | 95 | ISO 2 | + 23 / 38 | +10/25 | + 25 /40 | | |
| M3.0 | x 0.5 | 6H | 100 | 100 | ISO 2 | + 24 / 40 | +10/25 | + 25 /40 | | |
| M3.5 | x 0.6 | 6H | 112 | 90 | ISO 2 | + 27 / 45 | +10/25 | + 25 /40 | | |
| | 0.7 | 211 | 440 | 440 | 100.0 | 00 / 10 | | 00.440 | | |
| M4.0 | x 0.7 | 6H | 118 | 118 | ISO 2 | + 29 / 48 | | + 20 /40 | | |
| M5 | x 0.8 | 6H | 125 | 125 | ISO 2 | +30/50 | | + 20 /40 | | |
| M6 | x 1.0 | 6H | 150 | 120 | ISO 2 | + 35 / 59 | | + 20 /40 | | |
| M7 | x 1.0 | 6H | 150 | 120 | ISO 2 | + 35 / 59 | | + 20 /40 | | |
| M8 | x 1.25 | 6H | 160 | 130 | ISO 2 | + 38 / 63 | | + 20 /40 | +40/60 | |
| M10 | x 1.5 | 6H | 180 | 140 | ISO 2 | + 42 / 70 | | + 20 /40 | +40/60 | |
| M12 | x1.75 | 6H | 200 | 160 | ISO 2 | + 48 / 80 | | | + 40 / 60 | +60/8 |
| M14 | x 2.0 | 6Н | 200 | 170 | ISO 2 | + 48 / 80 | | | + 40 / 60 | +60/8 |
| M16 | x 2.0 | 6Н | 212 | 170 | ISO 2 | | | | + 40 / 60 | +60/8 |
| | | | | | | +51/85 | | | , | |
| M18 | x 2.5 | 6H | 224 | 190 | ISO 2 | +54/90 | | | +40/60 | +60/8 |
| M20 | x 2.5 | 6H | 224 | 190 | ISO 2 | +54/90 | | | +40/60 | + 60 / 8 |
| M22 | x 2.5 | 6H | 224 | 190 | ISO 2 | + 54 / 90 | | | +40/60 | + 60 / 8 |
| M24 | x 3.0 | 6H | 265 | 200 | ISO 2 | +64/106 | | | + 40 / 60 | + 60 / 8 |

P limits; they stock the smaller P limit for SP Taps, and the larger P limit for PO taps. Where there is only the one "P" limit; it is the same limit for both SP & PO Taps

The ISO metric system of tap tolerances comprises three classes of tap sizes which are calculated from the Grade 5 nut tolerance, irrespective of the nut grade to be cut as follows:

ISO, Class 1 – Class 2 – Class 3

The tolerances of these three classes are determined in terms of a tolerance unit t, the value of which is equal to the pitch tolerance value TD2 grade 5 of nut (extrapolated up to pitch 0.2mm):

t = TD, grade 5

The value of the tap pitch diameter tolerance is the same for all three classes 1, 2 and 3: it is equal to 20% of t.

The position of the tolerance of the tap with respect to the basic pitch diameter results from the lower deviation the values of which are

(see Figure 3):

for tap class 1: + 0.1 t for tap class 2: + 0.3 t for tap class 3: + 0.5 t Choice of tolerance class of the tap with respect to the class of thread to be produced.

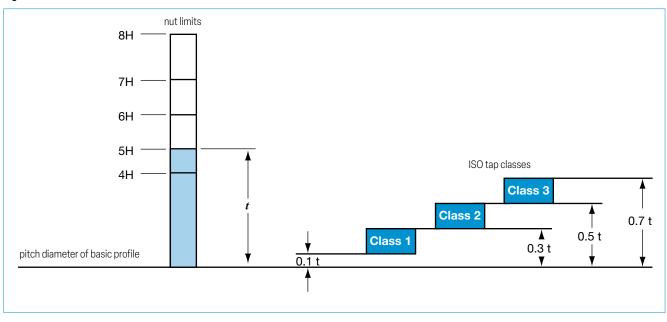
Unless otherwise specified, the taps of classes 1 to 3 will generally be used for the manufacture of nuts of the following classes:

ISO, Class 1: for nuts of limits 4H and 5H

ISO, Class 2: for nuts of limits 6H and 5G

ISO, Class 3: for nuts of limits 7H - 8H and 6G.

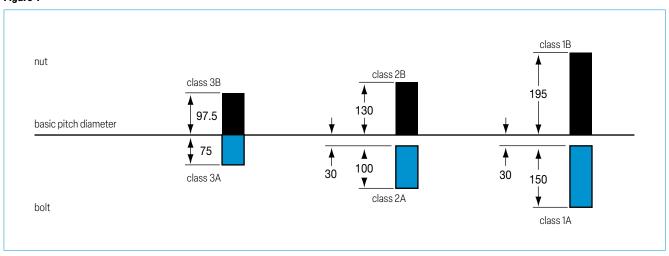
Figure 3



This system is well known. It has now been accepted by ISO as the recommended tolerance for ISO inch threads down to 0.06 inch nominal diameter. The arrangement of the allowance and the various classes of pitch diameter tolerance for a normal length of engagement of the mating threads is shown in this

The pitch diameter tolerance for Class 2A bolts is shown as 100 units, and the fundamental deviation and other tolerances are shown as percentages of the Class 2A tolerance. Figure 4.

Figure 4



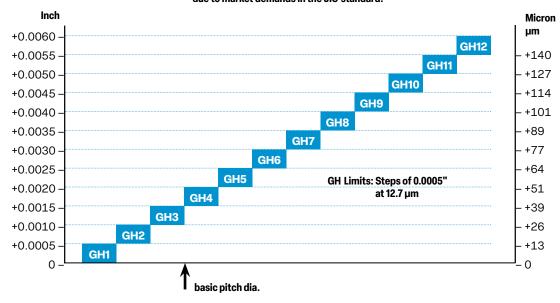
Unified Taps The "GH" System

This system provides for a range of pitch diameters for each size of tap: the height limit of pitch diameters being the basic pitch diameter plus increments or units of .0005". It is designated by the letter "GH" followed by a numeral indicating the number or units applying to the particular "GH" size. The tap manufacturer's tolerance is applied as minus.

This is the limit which will normally be supplied. Alternative "GH" limits other than those shown in the price list can be made to special order.

GH Limits for JIS Roll Taps

GH Limits are applied to JIS Metric and Unified Thredflo Tap Threads due to market demands in the JIS standard.



For Sutton Tools Metric (mm) Roll / Fluteless Taps (Limit same as the "RH" & "G" Limits) GH Limits: Steps of 0.0127 mm

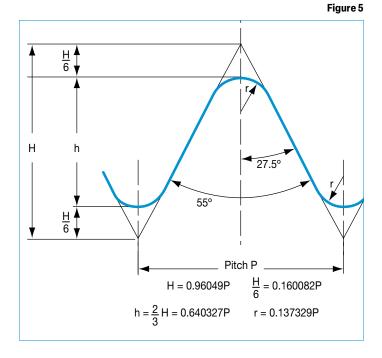
Upper limit: 0.0005" x N Lower limit: (0.0005" x N) - 0.0005

GH LIMITS

Basic Profile for Whitworth (BSW, BSF and WHIT.) Thread forms

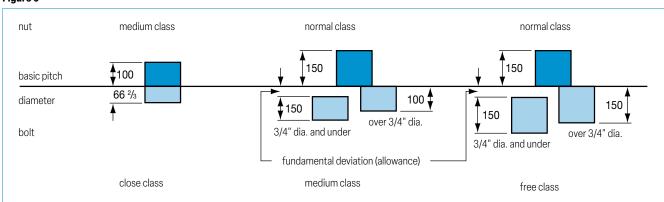
British Standard Whitworth Form

The sides of the thread form an angle of 55° with one another, and the top and bottom of the full triangle are truncated one-sixth of the height. The actual depth of the thread is equal to two-thirds of the height of the generating triangle and is equal to 0.6403 times the pitch. The crests and roots are rounded to a radius of 0.137329 times the pitch. **Figure 5**.



The Whitworth Screw Thread Tolerance System

Figure 6



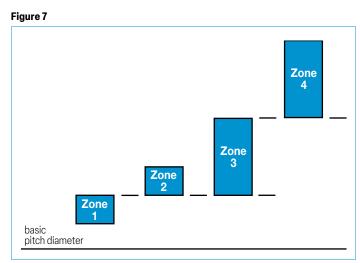
Pitch diameter tolerance zones of recommended combinations of classes of bolts and nuts having Whitworth screw threads. Figure 6.

British Tap Size Zone Limits

British Standard Zone 3 and Zone 4 limits are normally applied to Whitworth and BA taps.

The values for position and tolerances are formulated and must be obtained from the standard's tables.

The accompanying chart shows the zone limits relationship for ground threads. **Figure 7**.



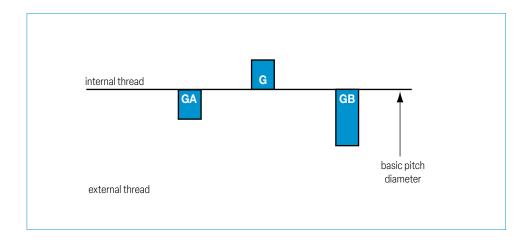
Technical Information ISO Pipe Tap Thread Systems



The International Standard Pipe Tap Thread System (ISO) has been derived from the original Whitworth gas and water pipe tap threads, formerly known as BSPF (Fastening) and BSPT (Taper), these systems have been so widely used throughout Europe and the United Kingdom that they have been metricated, whilst still retaining the Whitworth thread form. These popular thread systems are the basis for the ISO parallel "G" series and the taper "R" series, these systems are endorsed and in agreement with the current British and Australian standards. For comparison, the pitch diameter tolerance zones are given for both the parallel and taper systems.

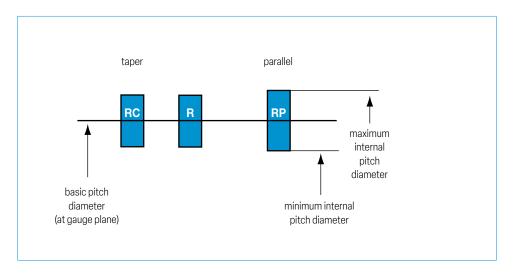
"G" Fastening Parallel Pipe Threads - ISO 228, AS1722 PT2 and BS2779.

This parallel thread system has only one positive internal thread tolerance and two classes of external tolerances. This series constitutes a fine series of fastening connecting pipe threads for general engineering purposes, the assembly tolerances on these threads are such as to make them unsuitable for pressure tight seal by the threads themselves. For the conveying of fluids, the seal may be produced by gaskets, flanges, or "O" rings.

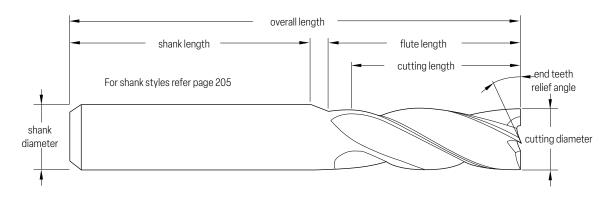


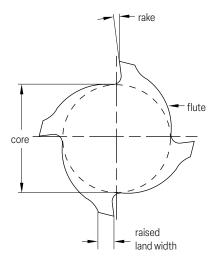
"R" Sealing Taper Pipe Threads – ISO 7, AS1722 PT1 and BS21. The taper rate is 1-16 on diameter.

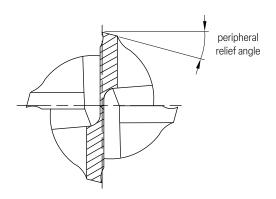
This series is for tubes and fittings where pressure tight joints are made by threads, these threads therefore must have a full form profile (no truncations). The series include a taper external thread (R) for assembly with either taper internal (Rc) or parallel internal (Rp) threads. The Rp series has a unilateral tolerance (+/-) which normally requires a special below basic low limit tap, to allow for sizing deviations at the start of the internal thread, the size is gauged at this position, with an Rc taper gauge. The low limit Rp tap size, allows a minimum accommodation length to be machined, with an equivalent material saving possible.



Endmill Definitions







Conventional milling versus climb milling

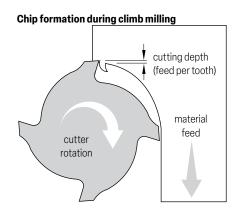
A milling cutter can cut in two directions, sometimes known as climb or conventional.

Conventional milling: The depth of the cut starts at zero thickness, and increases up to the maximum. The cut is so light at the beginning that the tool does not cut, but slides across the surface of the material, until sufficient pressure is built up and the tooth suddenly bites and begins to cut. This deforms the material (at point A on the diagram, left), work hardening it, and dulling the tool. The sliding and biting behaviour leaves a poor finish on the material.

cutting depth (feed per tooth) material feed material to be removed by the next tooth

Conventional milling. Point A become work hardened

Climb milling: Each tooth engages the material at a definite point, and the width of the cut starts at the maximum and decreases to zero. The chips are disposed behind the cutter, leading to easier swarf removal. The tooth does not rub on the material, and so tool life may be longer. However, climb milling can apply larger loads to the machine, and so is not recommended for older milling machines, or machines which are not in good condition. This type of milling is used predominantly on mills with a backlash eliminator.



| Туре | Description | Application | Illustration |
|---------|--|-------------|--------------|
| N | Finishing Form | | |
| W | Slotting & Finishing - Use in soft materials, quick spiral 45° up to 600 N/mm² | | |
| VA | Optimised geometry for Austentic Stainless Steels & other long chipping materials up to 1000 N/mm² | | |
| AI & CU | For slotting wrought aluminium alloys with efficient chip evacuation, due to high relief angles and 40° spiral | | |
| NR | Normal Roughing Form - general purpose | | |
| NF | Semi Roughing Form - Ideally suited to soft, long chipping materials. | | |
| WR | Coarse Form - ideally suited to soft, non-ferrous materials. | | |
| HR | Fine Pitch Roughing Form - ideally suited to hard, short chipping materials | | |
| HRS | Special Fine Pitch Roughing Form - Universal use | | |
| Ti | Wave Form - ideally suited to titanium & nickel alloys | | |
| STF | Special tooth form - Semi Roughing Form, ideally suited to materials up to 1400 N/mm² | | |

Technical Information Reamers

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Hints on use

Feeds

In reaming, feeds are usually much higher than those used for drilling. The amount per feed may vary with the material, but a good starting point would be between 0.038mm and 0.10mm per flute per revolution. Too low a feed may result in glazing, excessive wear, and occasionally chatter. Too high a feed tends to reduce the accuracy of the hole and may lower the quality of the finish. The basic idea is to use as high a feed as possible and still produce the required accuracy and finish.

Stock to be removed

For the same reason, insufficient stock for reaming may result in a burnishing rather than a cutting action. It is very difficult to generalise on this phase as it is closely tied with the type of material the finish required, depth of hole, and chip capacity of the reamer. For machine reaming 0.20mm for a 6mm hole, 0.30mm for a 12mm hole, and 0.50mm for a 50mm hole, would be a typical starting point guide.

For hand reaming, stock allowances are much smaller, partly because of the difficulty in hand forcing the reamer through greater stock. A common allowance is 0.08mm to 0.13mm.

Speeds

The most efficient speed for machine reaming is closely tied in with the type of material being reamed, the rigidity of the set-up, and the tolerance or finish required. Quite often the best speed is found to lie around two-thirds the speed used for drilling the same material.

A lack of rigidity in the set-up may necessitate slower speeds, while occasionally a very compact, rigid operation may permit still higher speeds.

When close tolerances and fine finish are required it is usually found necessary to finish the reamer at considerably lower speeds.

In general, reamers do not work well when they chatter. Consequently, one primary consideration in selecting a speed is to stay low enough to eliminate chatter. Other ways of reducing chatter will be considered later, but this one rule holds: SPEEDS MUST NOT BE SO HIGH AS TO PERMIT CHATTER.

The following charts gives recommended surface meter per minute values which may be used as a basis from which to start.

| | m/min |
|------------------------------|---------|
| Aluminium and its alloys | 20 – 35 |
| Brass and Bronze, ordinary | 20 – 35 |
| Bronze, high tensile | 18 – 22 |
| Monel Metal | |
| Cast Iron, soft | 22 – 35 |
| Cast iron, hard | 18 – 22 |
| Cast Iron, chilled | 7 – 10 |
| Malleable Iron | 18 – 20 |
| Steel, Annealed | 13 – 18 |
| Steel, Alloy | 12 – 13 |
| Steel, Alloy 300-400 Brinell | |
| Stainless Steel | 5 – 12 |

Chatter

The presence of chatter while reaming has a very bad effect on reamer life and on the finish of the hole. Chatter may be the result of several causes, some of which are listed:

- 1. Excessive speed.
- 2. Too much clearance on reamer.
- 3. Lack of rigidity in jig or machine.
- 4. Insecure holding of work.
- 5. Excessive overhang of reamer in spindle.
- 6. Excessive looseness in floating holder.
- 7. Too light a feed.

Correcting the cause can materially increase both reamer life and the quality of the reamed holes

Coolants for Reaming

In reaming, the emphasis is usually on finish and a lubricant is normally chosen for this purpose rather than for cooling. Quite often this means a straight cutting oil.

Limit of tolerance on cutting diameter

The tolerance on the cutting diameter measured immediately behind the bevel or taper lead for parallel reamers listed is M6 as specified in BS122-PT2-1964. It is not practicable to standardise reamer limits to suit each grade of hole and the limits chosen are intended to produce H7 holes.

| | | Diameter 1ge | | Cutting Edge Diameter | | | | |
|--------|---------------------|-----------------|---------------------|--------------------------|----------|-----------|----------|--|
| In | Inch | | mm | | Inch | | mm | |
| Over | Up to and including | Over | Up to and including | High + | Low + | High + | Low + | |
| 0.0394 | 0.1181 | 1 | 3 | 0.0004 | 0.0001 | 0.009 | 0.002 | |
| 0.1181 | 0.2362 | 3 | 6 | 0.0005 | 0.0002 | 0.012 | 0.004 | |
| 0.2362 | 0.3937 | 6 | 10 | 0.0006 | 0.0002 | 0.015 | 0.006 | |
| 0.3937 | 0.7087 | 10 | 18 | 0.0007 | 0.0003 | 0.018 | 0.007 | |
| 0.7087 | 1.1181 | 18 | 30 | 0.0008 | 0.0003 | 0.021 | 0.008 | |
| 1.1811 | 1.9085 | 30 | 50 | 0.0010 | 0.0004 | 0.025 | 0.009 | |
| 1.9085 | 3.1496 | 50 | 80 | 0.0012 | 0.0004 | 0.030 | 0.011 | |

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| APPLICATION TAP | - SPECIAL ENQUIRY |
|--|---|
| Customer No.: New Customer Company: Address: State / Province: Country: | Order No. |
| Tap Details | Quantity: |
| Basic Geometry Tool Material HSS HSSE PM-HSSE V3 PM-HSS C0 Thread Limit: NB: If special thread form, please supply details on separate drawing. d ₁ d ₂ l ₁ sq a/f | Coating Uncoated Steam Oxide TiN TiAIN TiCN Other Other Product No: Speed: |
| Workpiece Details Component: Material Group: Material Grade: | Machine Details Machine Type: Coolant: Tapping Attachment: CNC Neat Oil Tapping Chuck Semi Auto Mist / Dry Tension Manual Emulsion > 5% Compression |
| Characteristics of Material: Short Chipping Hole Type: Through Hole Tapping Hole Size: Drilled Cast Punched Hole Depth: | Machine Direction: Wertical Feed: Collet Chuck (length compensating) Oblique Mechanical Pneumatic Hydraulic Manual Rotating Chuck (length compensating) Warning Manual CNC Collet Chuck (length compensating) Apping Attachment Tapping Attachment Tapping Chuck (rigid) Collet Chuck (length compensating) Collet Chuck (length compensating) Mechanical Pneumatic Hydraulic Manual Manual Collet Chuck (length compensating) Collet Chuck (length compensating) Collet Chuck (length compensating) Collet Chuck (length compensating) Manual Manual Collet Chuck (length compensating) Collet Chuck |
| Drawing / Notes | |

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APPLICATION HSS DRILLS - SPECIAL ENQUIRY New Customer ___ Order No. | | | | | | | | | | | Customer No.: Contact: Company: Phone: Address: State / Province: Fax: Country: Email: **Drill Details** Quantity: **Basic Geometry Tool Material:** HSS Tool Type: HSSE ☐ Drill PM-HSSE V3 Step Drill Countersinks other _____ ☐ Subland Drills **Plus Coating:** Yes No Core Drills ☐ Centre Drills ☐ TiN TiCN TiAIN Steam Oxide Total Length (mm): Number of Steps: other _____ ☐ Without Yes No Plus Internal Cooling: ☐ With ______steps \Box d_s Point Design Shank Design: Reinforced Point Geometry: Without Flat Relieved Cone For Grey Cast Iron ☐ With Flat Parallel Straight Shank Centre Point Morse Taper Facet Point Grind other other _____ Special Point Grind, Form: \square A □в \Box c □RH Spiral: **Drawing / Notes**

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APPLICATION CARBIDE DRILL - SPECIAL ENQUIRY New Customer Customer No.: Order No. | Company: Contact: Phone: Address: State / Province: Fax: Email: Country: **WITHOUT Internal Cooling WITH Internal Cooling SOLID CARBIDE DRILL WITHOUT STEP** Quantity: Quantity: **** Carbide grade (specify if known) (specify if known) Norm-Ød₁ (4 - 20mm)(3 - 20mm)Shank-Ød₂ (DIN 6535) (DIN 6535) Shank length I₃ (DIN 6535) (DIN 6535) ПНА ПНА HE Shank form HE (DIN 6535) (DIN 6535) Drilling depth I₃ (maximum 7 x D) (maximum 7 x D) Flute length I₂ (9.5 – 155mm) (9.5 - 155mm) Total length I₁ (60 - 205mm) (60 - 205mm) □ 120° □ 130° ☐ 120° ☐ 130° ■ 140° ☐ 140° Point angle Point geometry (specify if known) (specify if known) Uncoated TiN Uncoated Surface finish/coating ☐ TiCN ☐ TiAN ☐ AICrN ☐ TiCN ☐ TiAN ☐ AICrN □ TiN Cost per tool **SOLID CARBIDE STEP DRILL** Quantity: Quantity: Carbide grade (specify if known) (specify if known) Step-Ød₁ (4 - 20mm)(3 - 20mm)Body-Ød₂ (4 - 20mm)(3 - 20mm)Shank-Ød₃ (DIN 6535) (DIN 6535) Shank length I₃ (DIN 6535) (DIN 6535) HE HE Shank form □ HA ПНА (DIN 6535) (DIN 6535) Step length I₄ (3 - 100mm) (3 - 100mm) Drilling depth I₃ (maximum 7 x D) (maximum 7 x D) Flute length I₂ (9.5 - 155mm) (9.5 - 155mm) Total length I₁ (60 - 205mm) (60 - 205mm) ☐ 120° ☐ 130° ☐ 140° ☐ 120° ☐ 130° ☐ 140° Point angle ☐ 60° □90° ☐ 60° □ 90° ☐ 120° Step angle ☐ 120° Point geometry (specify if known) (specify if known) Uncoated Uncoated Surface finish/coating TiN ☐ TiCN ☐ TiAN ☐ AICrN □TiN ☐ TiCN ☐ TiAN ☐ AICrN \$ Cost per tool

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APPLICATION MILLING - SPECIAL ENQUIRY New Customer Order No. | | | | | | | | | | Customer No.: Company: **Contact:** Phone: Address: State / Province: Fax: Country: Email: **Endmill Details** Quantity: **Basic Geometry Plus Internal Cooling** Range (Ø 4 - 20mm)Norm-Ød₂ (3 - 20mm)**Plus Coating** Yes No Shank-Ød2 to DIN 6535 (4 - 20mm) ☐ TIN ☐ TICN ☐ TIAN ☐ AICTN (Ø 4 – 20mm) Shank length I₃ to DIN 6535 mm Total length $I_1 Ø 3 - 10mm$ (28 - 100mm) **Tool Material** Specify grade (if known) from Ø 10 - 20mm (56 - 150mm) ☐ Carbide Cutting length $I_2 \emptyset 3 - 10 \text{mm}$ (3 - 40mm)□PM-HSSE from Ø 10 – 20mm (10 - 65mm)☐ HSS-Co Helix angle $w_2 \emptyset 3 - 6mm$ (20° – 45°) HSS from Ø 6 – 20mm $(20^{\circ} - 55^{\circ})$ No. of cutting edges Ø3 – 6mm (2 - 4mm)**Detail Regarding Application** from Ø6 - 20mm (2 - 6mm)Range of applications from Ø 16 – 20mm (2 - 8mm)Material description Material hardness (N/mm² or HRC) Shank Design Application types Straight Shank (DIN 6535) □HE ☐ Slotting Roughing **Peripheral Geometry** Finishing Copy milling Finishing endmills (Ø 3 – 20mm) \square N with Chip Breaker Roughing endmills **Drawing / Notes** Fine ☐ Coarse (Ø 6 – 20mm) **Face Geometry** Point angle w $(180^{\circ} + 5^{\circ})$ Yes □No **Cutting to Centre Corner Preparation** Yes □No Sharp edge Corner protection mm x 45° (Ø 0.03 – 1.5mm) Corner radius $mm \times d_{1} (0.3 - 2/3mm)$ Ballnose ☐ Yes □No Sharp edge Corner Corner radius Ballnose protection

